

Introduction of cavity coupler tuning

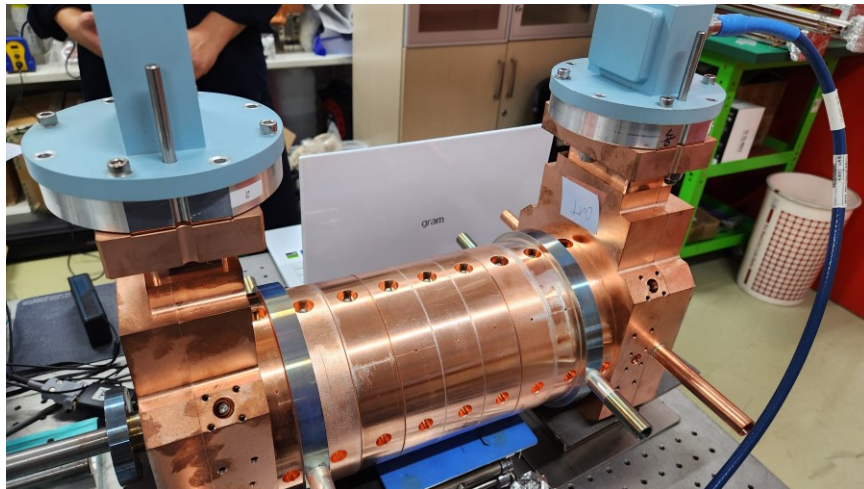
The classical kyhl method

Post-Brazing Verification

Brazing timeline, helium leak test, and pre-tuning S11 measurement.

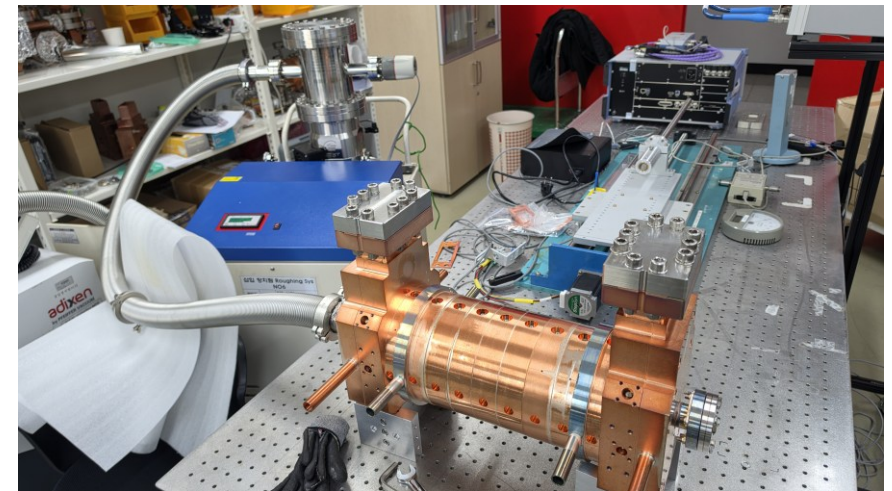
Brazing timeline

- 2025. 08. In/output coupler presentation (half brazing)
- 2025. 11. Re-measurement and full brazing
- 2026. 03. Leak test
- 2026. 03~04. S_{11} measurement (No tuning)



Helium leak test

- No leak detected.

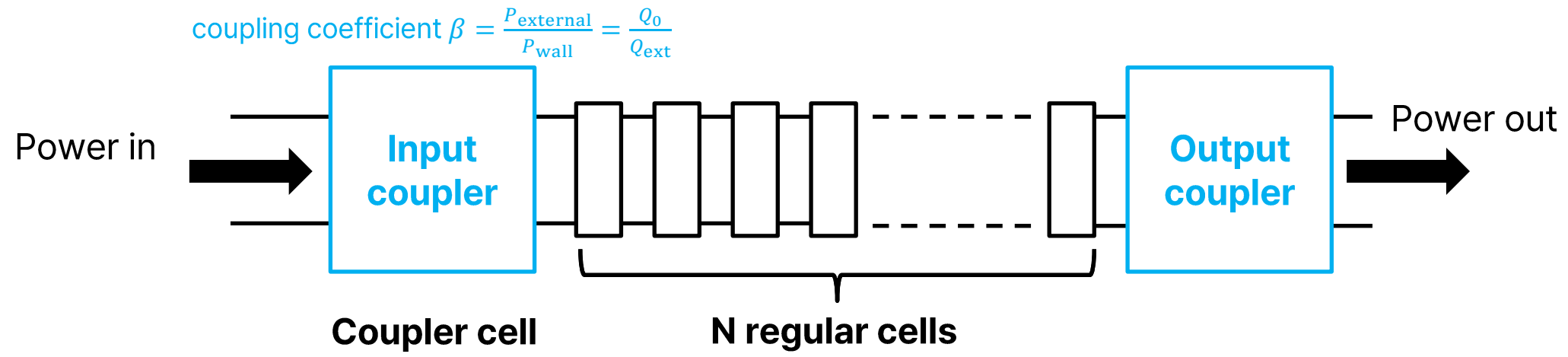
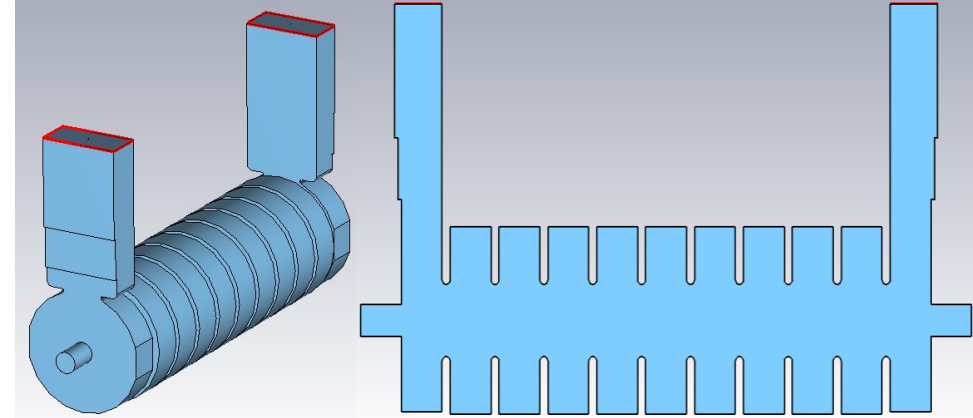


Coupler Role

The coupler controls RF power transfer and strongly affects cavity performance.

Why the coupler matters

- Impedance matching
 - Transfer RF power into and out of the cavity.
 - Coupling coefficient and external Q.
 - Mode purity (final resonant frequency).



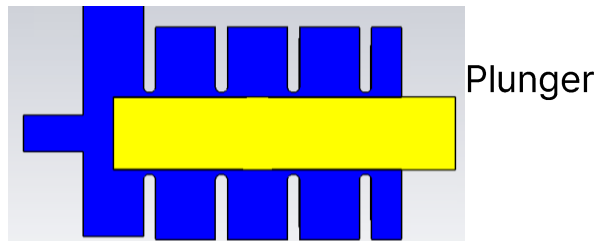
Method: kyhl method (Impedance matching method)

Frequency tuning based on the coupled-cell model.

Method overview

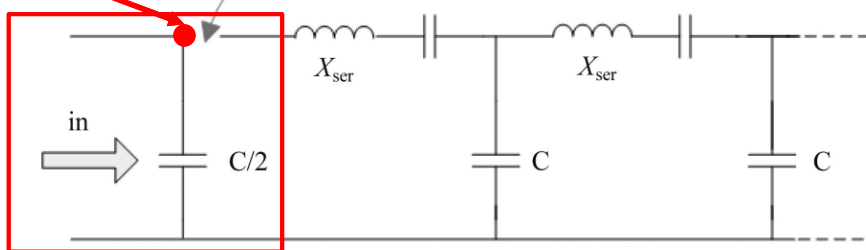
- Coupled-cell equivalent model
- Plunger-based freq. tuning
- Imp. matching of the coupler

0.5 cell

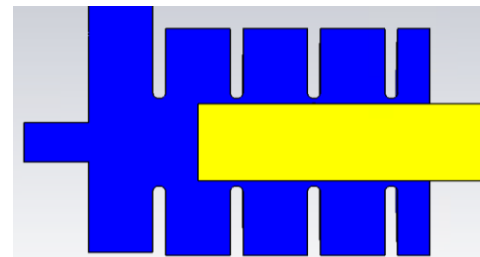


Coupler cell

arm disconnected

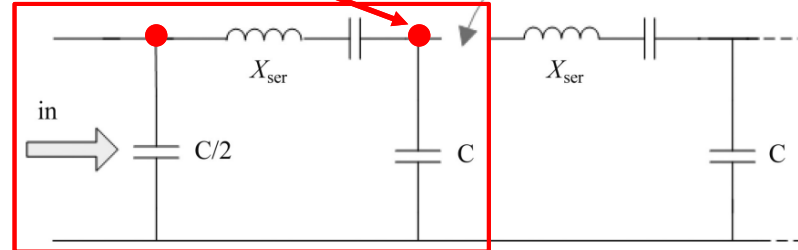


1.5 cell



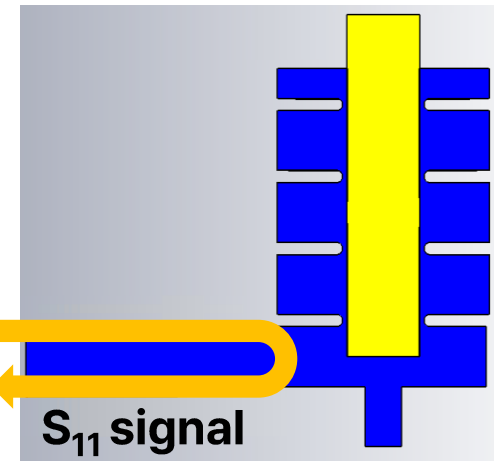
Reguler cell

arm disconnected



VNA

S_{11} signal



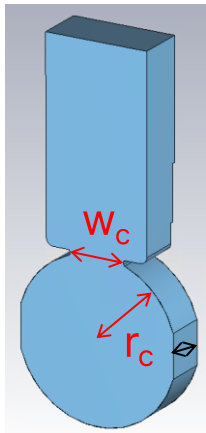
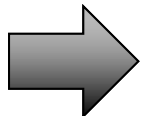
Tuning procedure

Tuning workflow

Goals

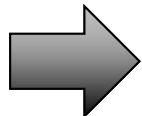
1. $\Delta f = f_{\text{target}} - f_{\text{shifted}} = 0$
2. Coupling coefficient $\beta \sim 1$

- $\Gamma = \frac{\beta - 1}{\beta + 1}$
- $|\Gamma| = 0$: No reflection
- $|\Gamma| = 1$: 100% reflection



Parameters

1. Coupler radius r_c
2. Coupler width w_c

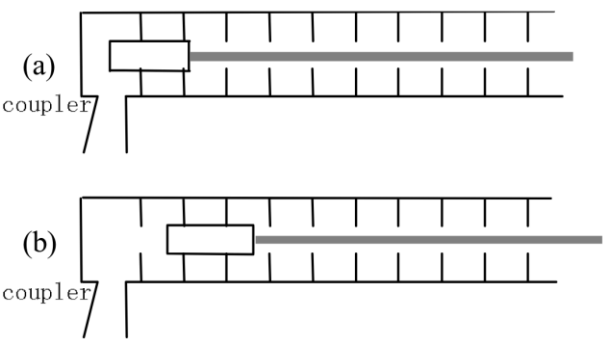


Kyhl's method

1. Detune three freq.
2. Phase $\Delta\Phi$ offsets



Zheng et al., Proc. PAC 2001, Chicago, 2001.



Wang et al., HEP&NP 30(6), 2006.

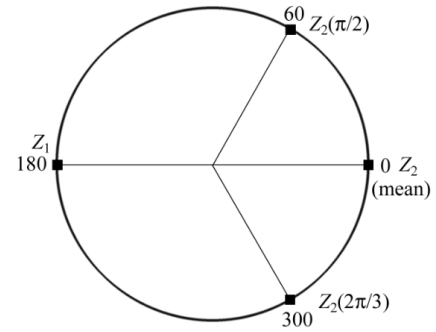


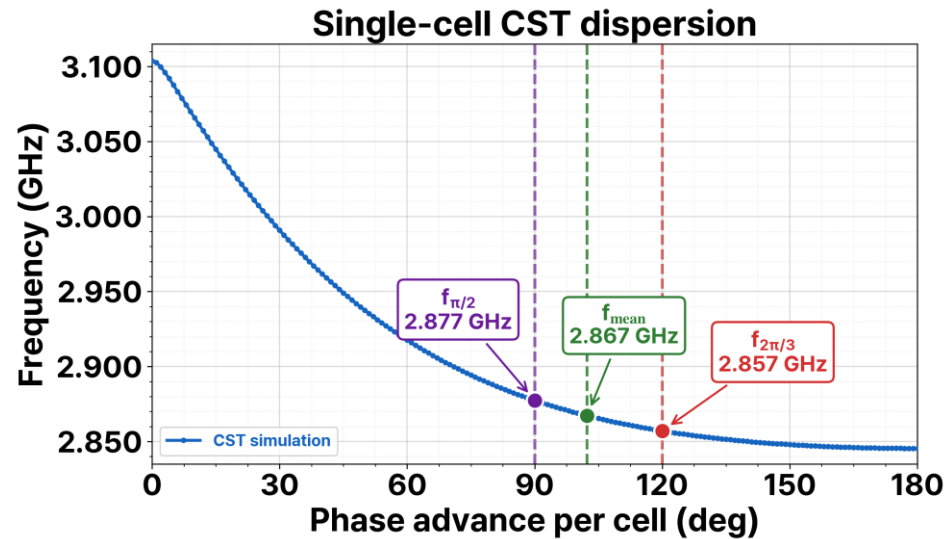
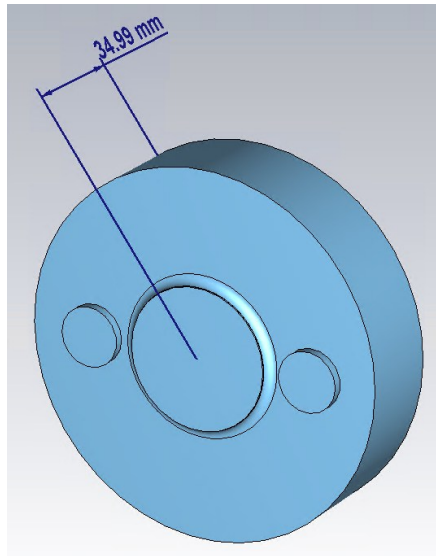
Fig. 1. Impedance points on a Smith Chart Plot.

Dispersion curve

$f_{\pi/2}$, $f_{2\pi/3}$, f_{mean}

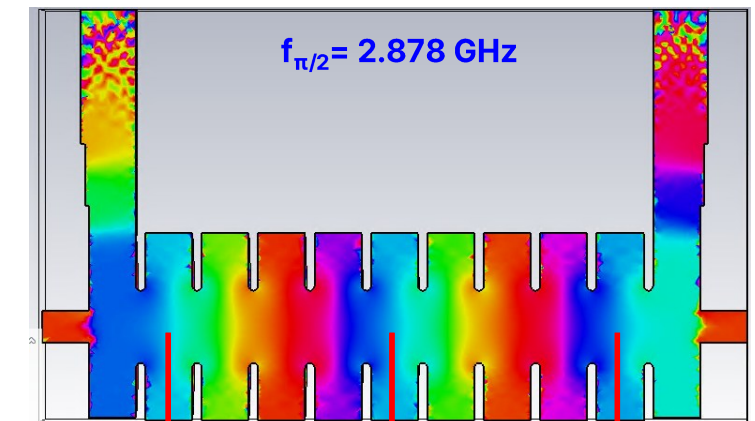
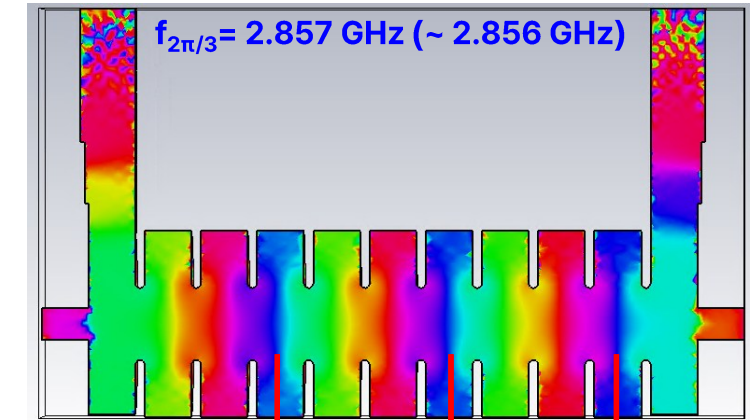
Freq. decision

1. Required freq.: $f_{2\pi/3}$, $f_{\pi/2}$, f_{mean}
2. CST simulation: Dispersion curve
3. Field distribution: $f_{2\pi/3}$, $f_{\pi/2}$ mode verification.



	$f_{2\pi/3}$	$f_{\pi/2}$	f_{mean}
Freq. (GHz)	2.857	2.877	2.867

<Phase propagation>

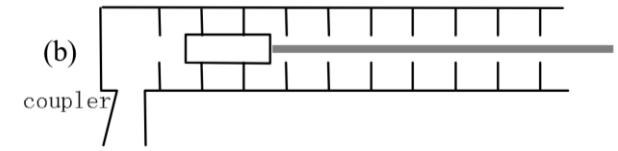
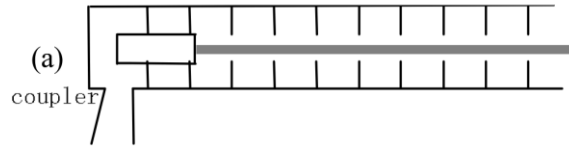


Simulation Comparison: S11 Dip Shift

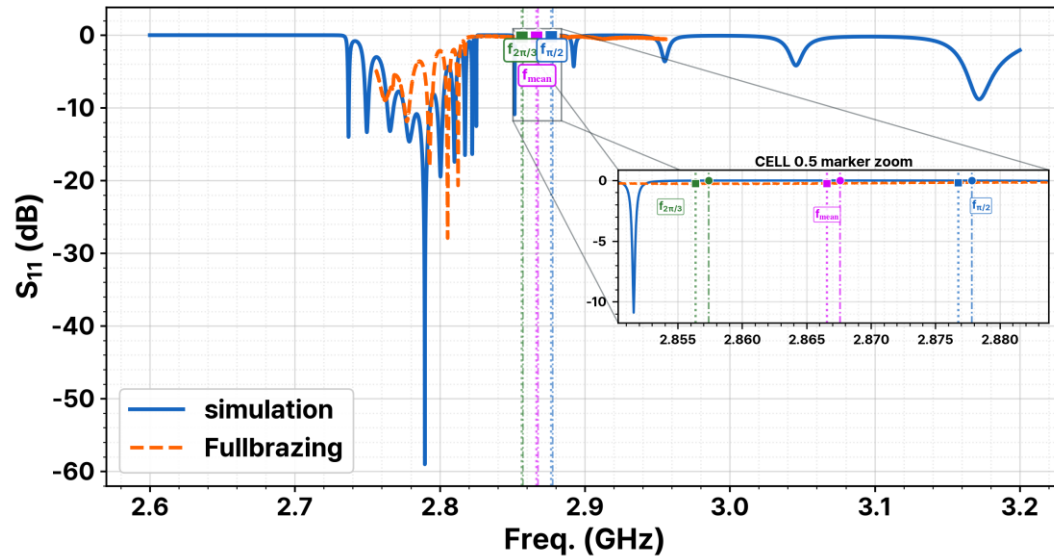
S11 were measured and analyzed to compare with the previous results.

Verification of three detuned short positions at the cell center (T=24.4 deg, H = 65%)

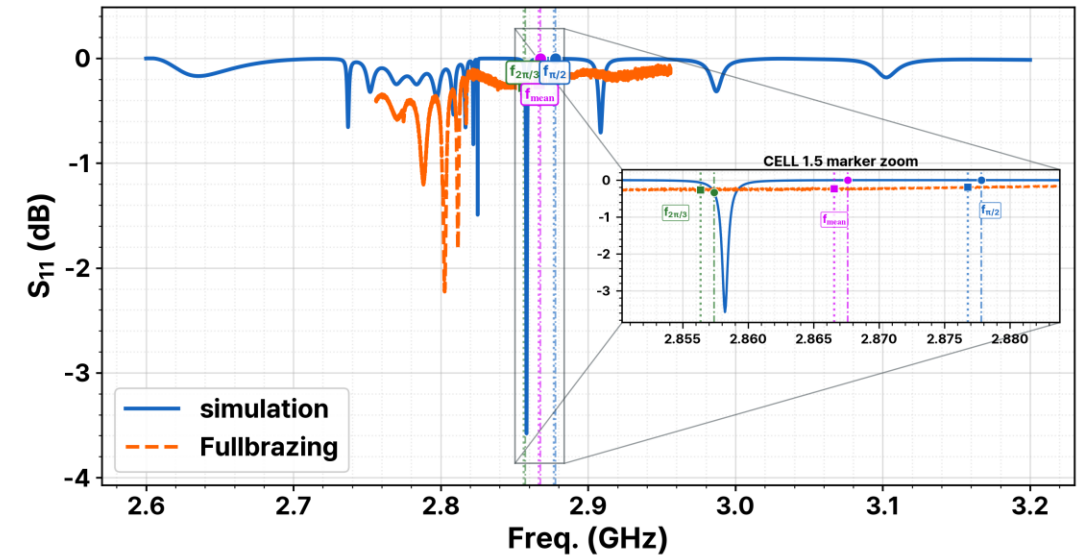
- $S_{11} = \Gamma$ @ one port network.
- $|\Gamma| \sim 1 \rightarrow 100\%$ reflection
- 0 dB $\rightarrow |S_{11}| \sim 1$



CELL 0.5: Sim260504 dB vs FullBrazing 260415



CELL 1.5: Sim260504 dB vs FullBrazing 260415



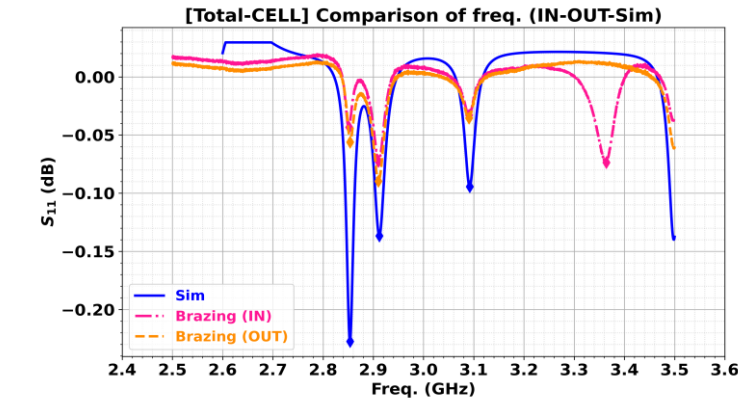
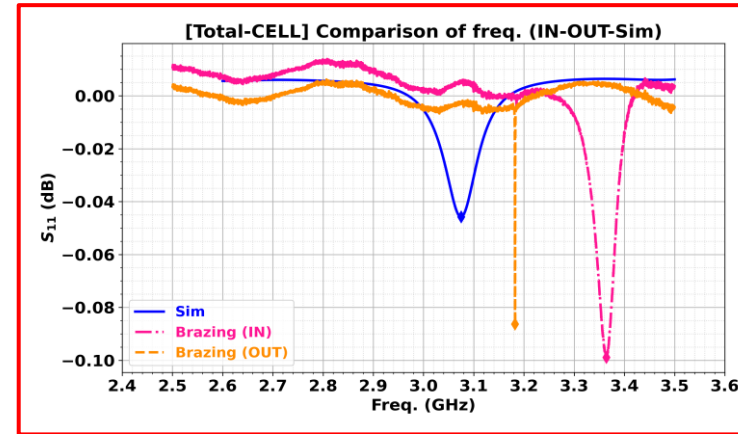
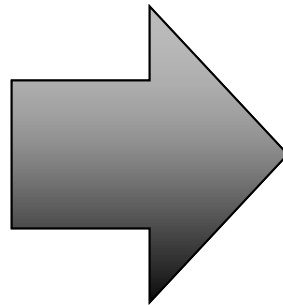
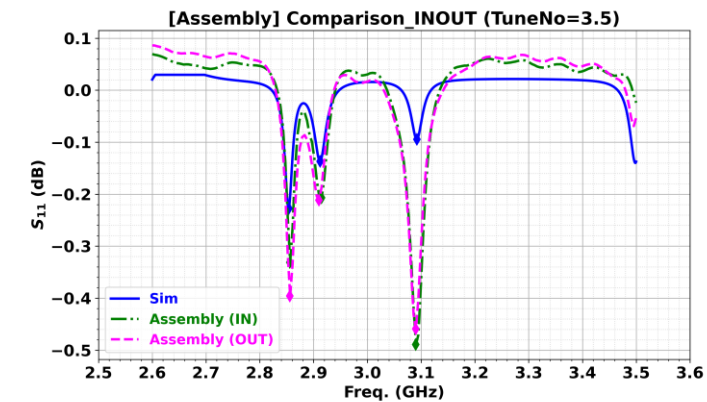
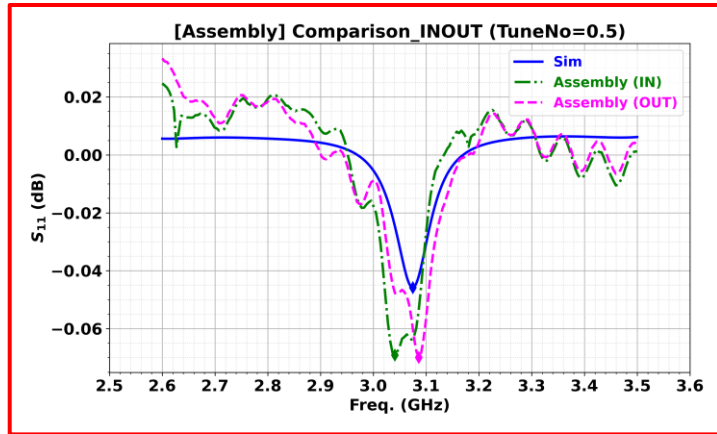
[Recap] Previous results



Frequency shift after input/output coupler brazing.

Comparison S_{11} results

- ~300 MHz frequency shift in the coupler cell.
- Mode excitation in the regular-cell region.



Assembly vs half	[IN] δf (MHz)	[OUT] δf (MHz)
$f_{\text{peak},1}$	323	96

Assembly vs half	[IN] δf (MHz)	[OUT] δf (MHz)
$f_{\text{peak},1}$	4	2
$f_{\text{peak},2}$	5	0
$f_{\text{peak},3}$	1	1

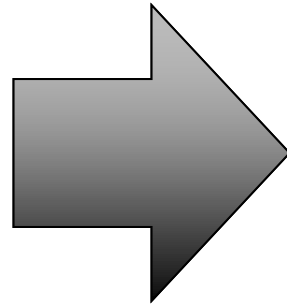
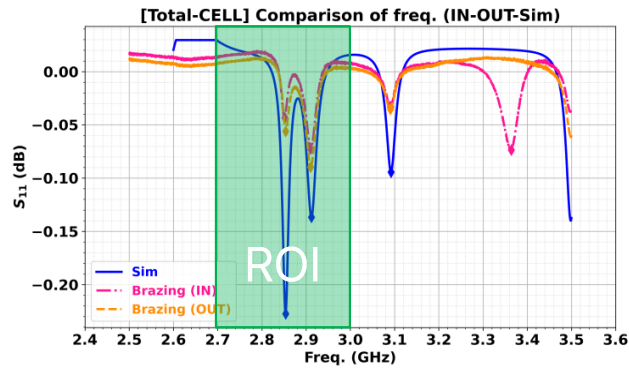
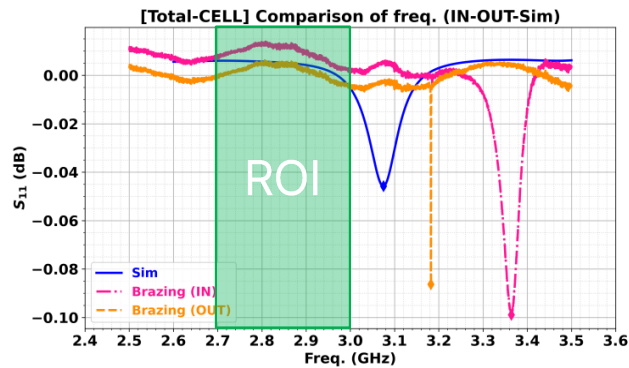
[Comparison] Half brazing vs Full brazing

S11 measurement and analysis for comparison with the previous results

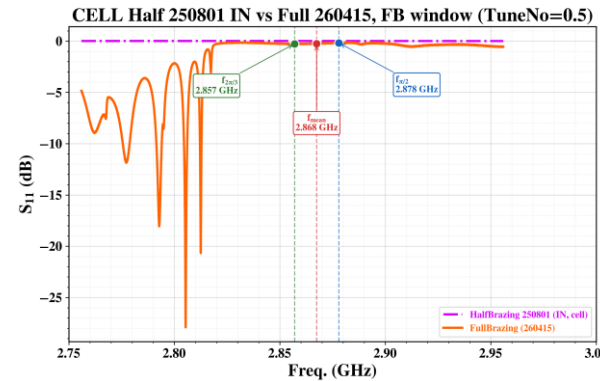


Comparison of Half and Full Brazing

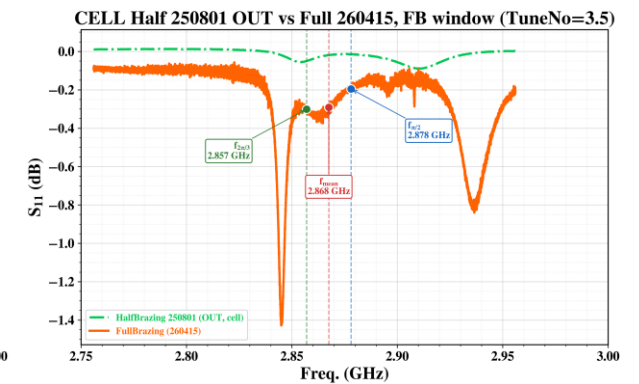
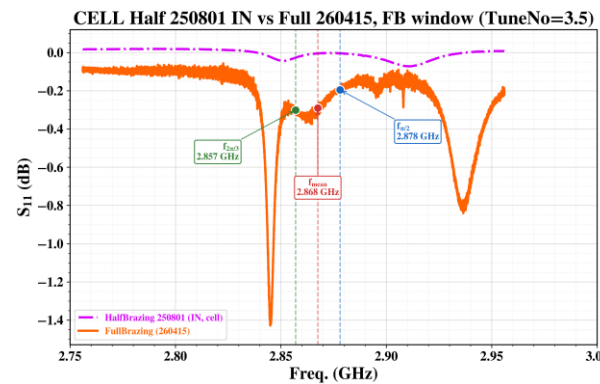
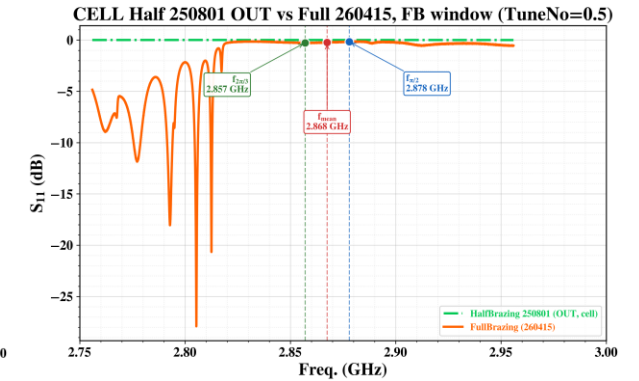
- Passband region of interest: $f_{\pi/2} \sim f_{2\pi/3}$
- Unwanted mode generation after full brazing.



Input half vs full



Output half vs full

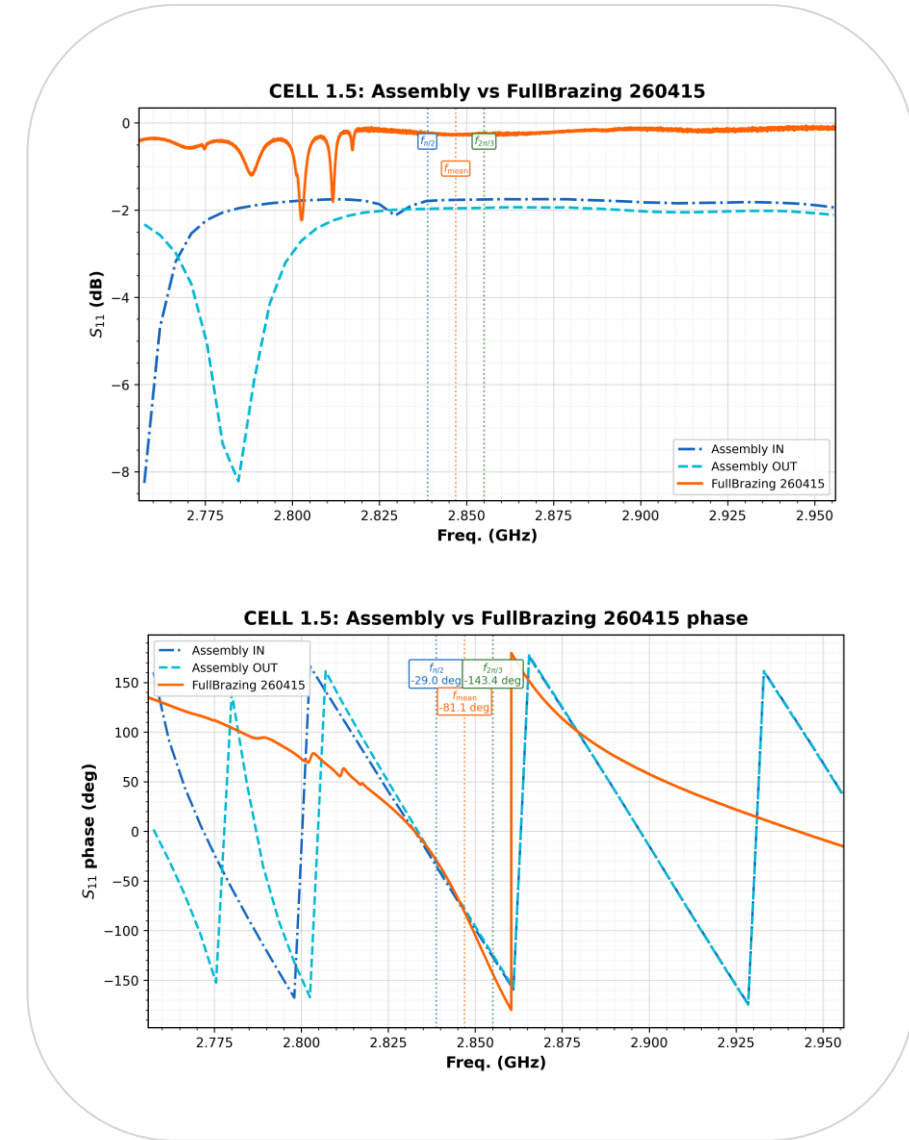
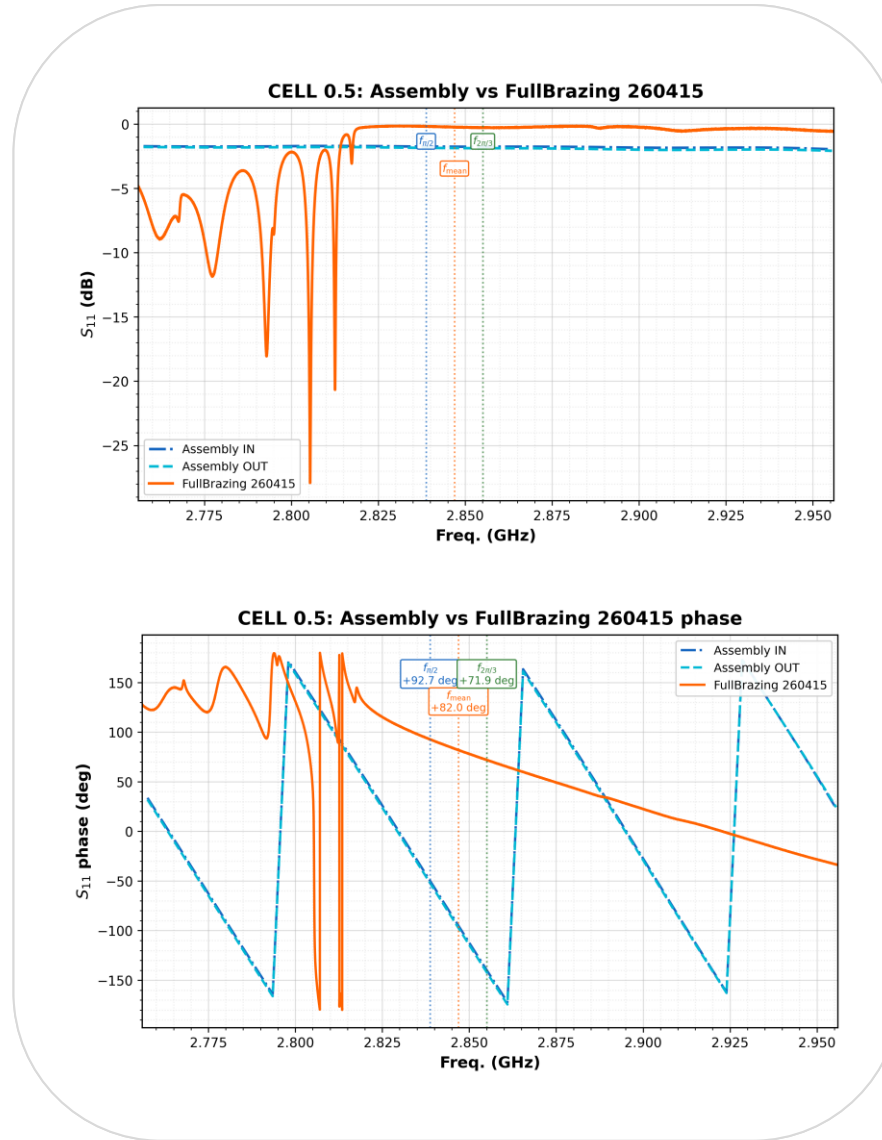


[Comparison] Assembly vs Full brazing



Phase comparison in ROI.

Phase measurement results



Method: kyhl method (Impedance matching method)

Frequency tuning based on the coupled-cell model.

Detune position decision

- Stage 1: check $\text{Re}(Z) = 0$ for three freq.
- Stage 2: confirm the phase spacing.
- $\Delta\Phi = 120$ deg for $f_{\pi/2}, f_{2\pi/3}$.
- $\Delta\Phi = 180$ deg for f_{mean} .

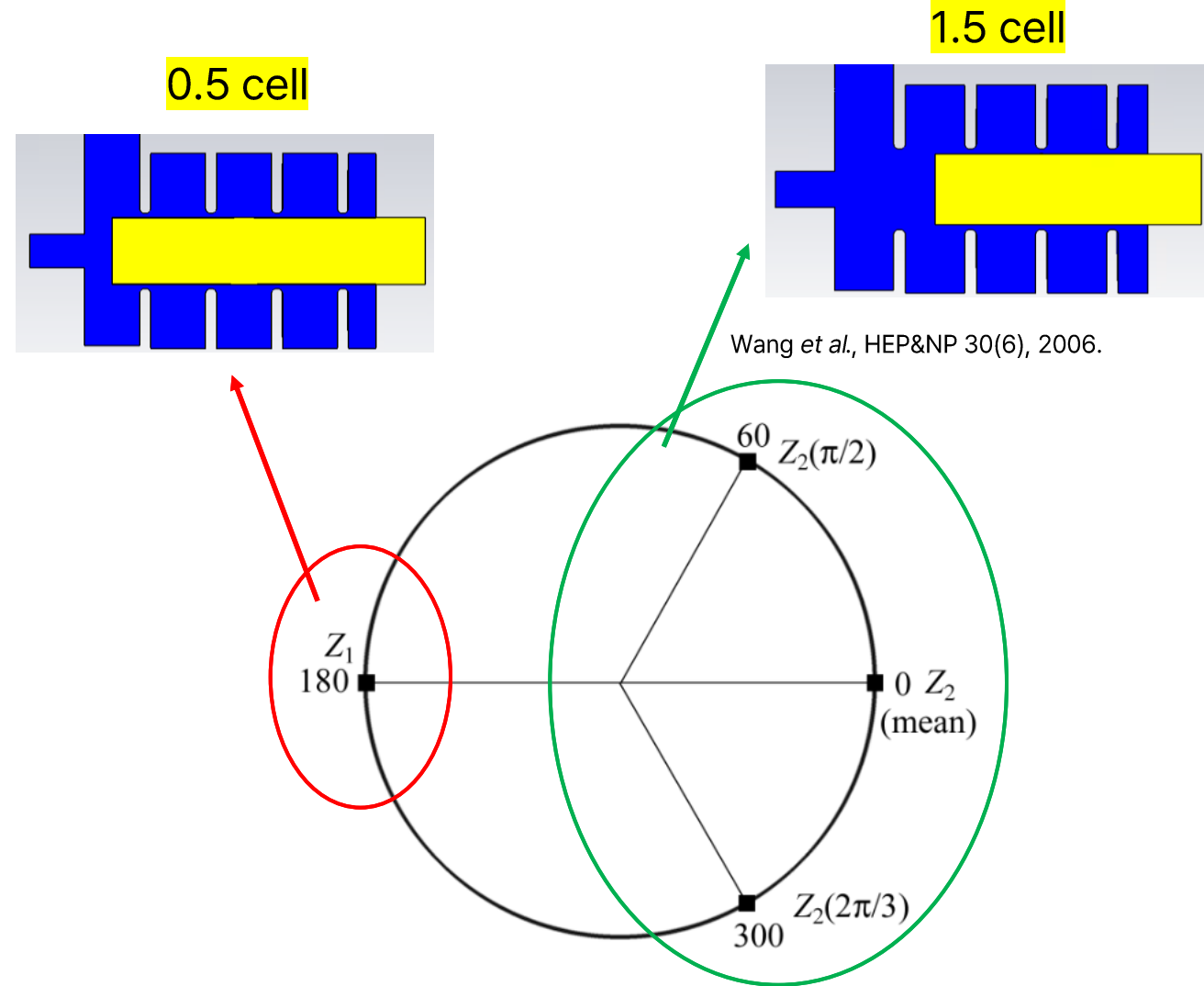
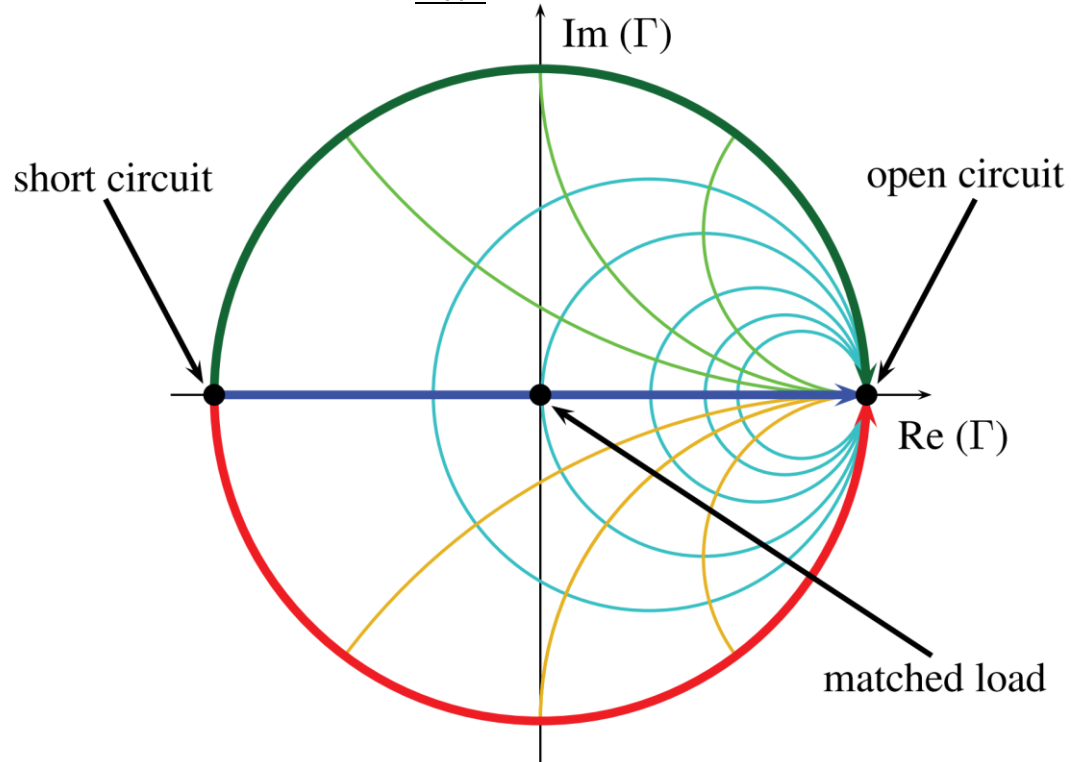


Fig. 1. Impedance points on a Smith Chart Plot.

Method: kyhl method (Impedance matching method)

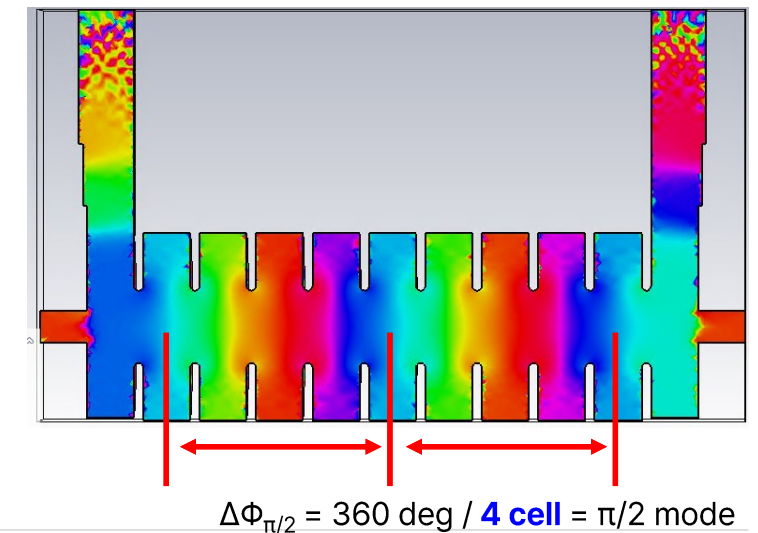
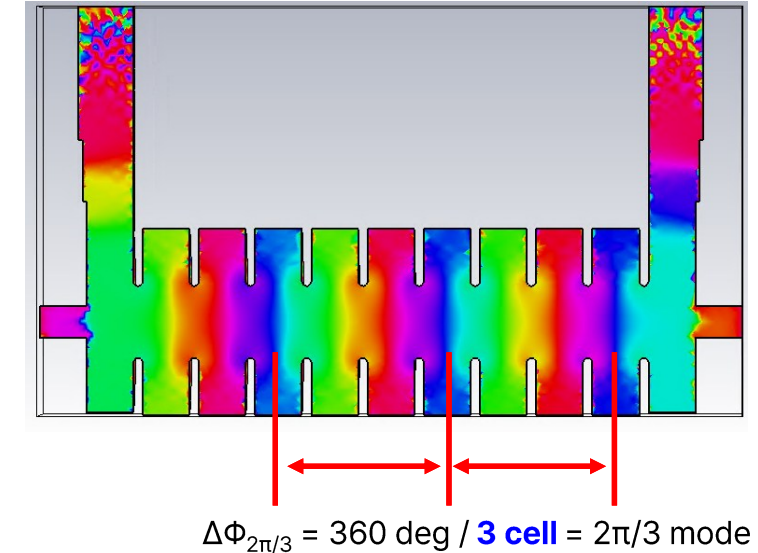
Frequency tuning based on the coupled-cell model.

Detune position desicion

- Propagation coefficient [rad/m]: $\beta_i = \frac{2\pi}{\lambda_{g,i}}$
- Phase propagation: $Z_{in}(f_i) = jZ_0 \tan(\beta_i l)$
- $f_{mean} = \frac{f_{2\pi/3} + f_{\pi/2}}{2}$

Freq.	cell phase advance $\beta_i l$	transformed Z_{in}
$f_{\pi/2}$	90 deg	$jZ_0 \tan(\beta_i l + 90)$
f_{mean}	105 deg	$jZ_0 \tan(\beta_i l + 105)$
$f_{2\pi/3}$	120 deg	$jZ_0 \tan(\beta_i l + 120)$

- ?
 - $\Delta\Phi = 120$ deg for $f_{\pi/2}, f_{2\pi/3}$.
 - $\Delta\Phi = 180$ deg for f_{mean} .



[Simulation Comparison] Detuning Analysis from S11 Markers



S11 marker positions and phase vectors from simulation and full-brazing cases

Wang *et al.*, HEP&NP 30(6), 2006.

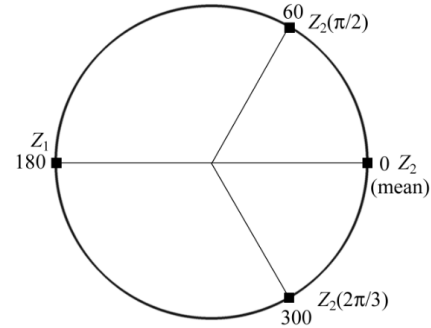
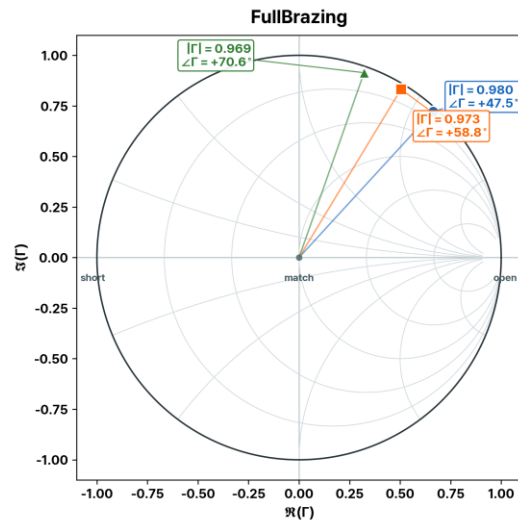
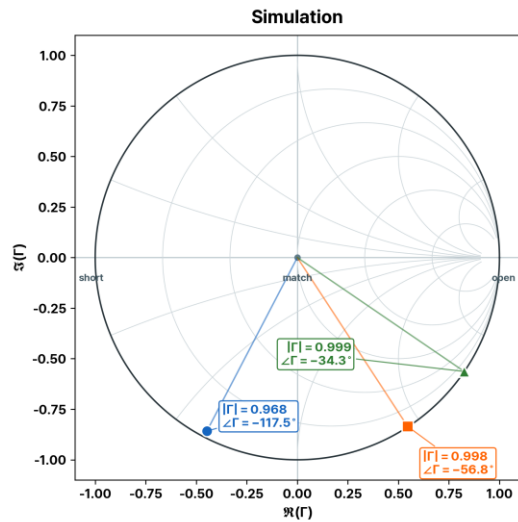


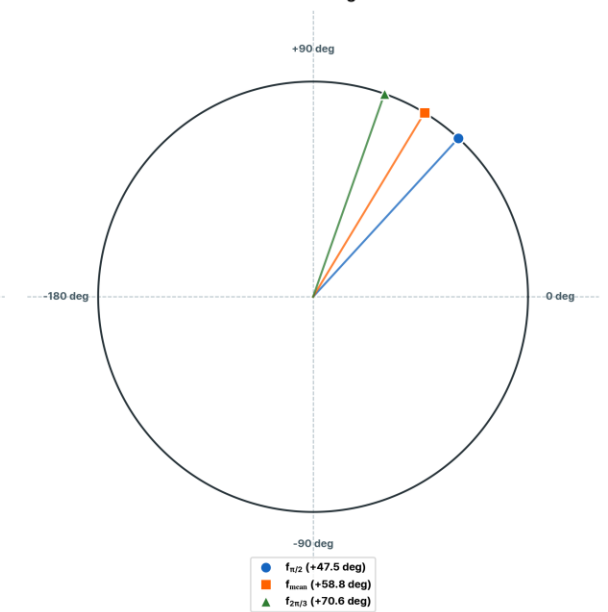
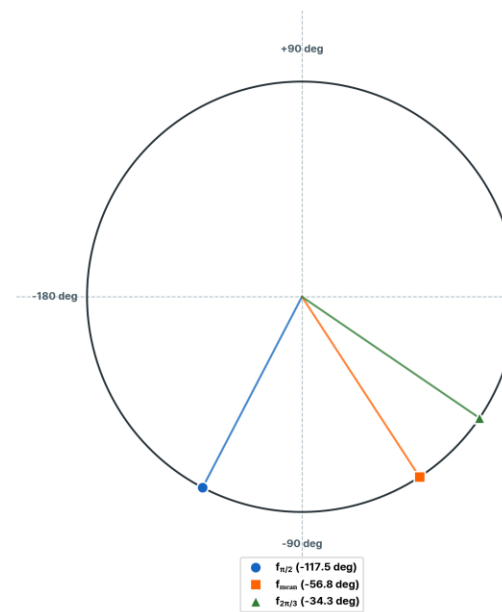
Fig. 1. Impedance points on a Smith Chart Plot.

Marker S11 on Smith chart: CELL 0.5



● $f_{\pi/2}$ ■ f_{mean} ▲ $f_{2\pi/3}$

Marker phase on S11 unit circle: CELL 0.5



● $f_{\pi/2}$ (-117.5 deg)
■ f_{mean} (-56.8 deg)
▲ $f_{2\pi/3}$ (-34.3 deg)

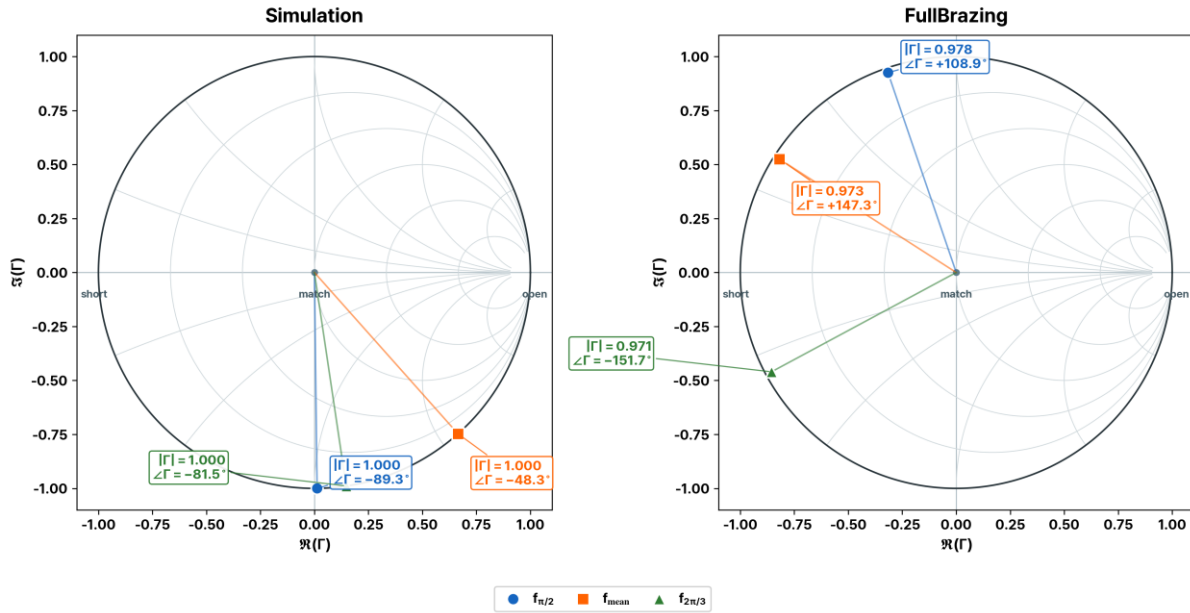
● $f_{\pi/2}$ (+47.5 deg)
■ f_{mean} (+58.8 deg)
▲ $f_{2\pi/3}$ (+70.6 deg)

[시뮬레이션 비교] Cell 1.5/2.5 에서의 detune 결과

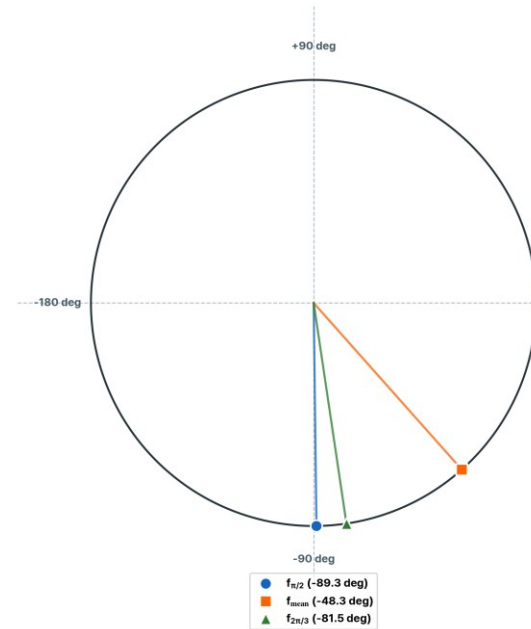


이전 결과와의 비교를 위한 S_{11} 값 측정&분석 수행.

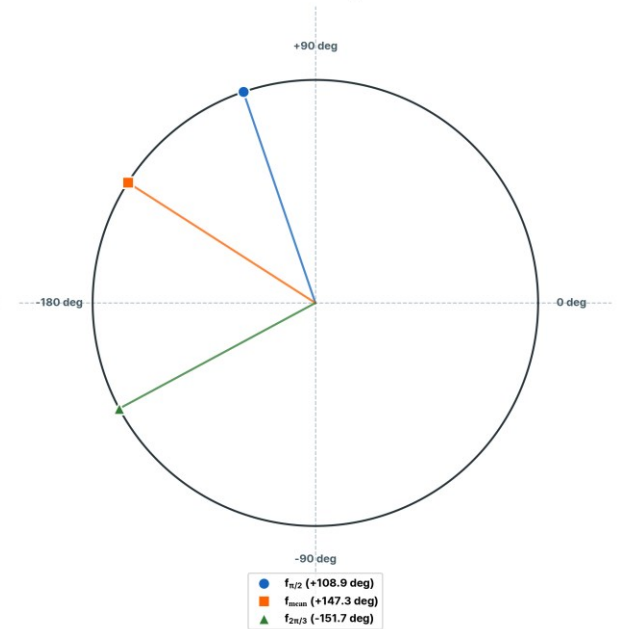
Marker S11 on Smith chart: CELL 1.5



Simulation Marker phase on S11 unit circle: CELL 1.5



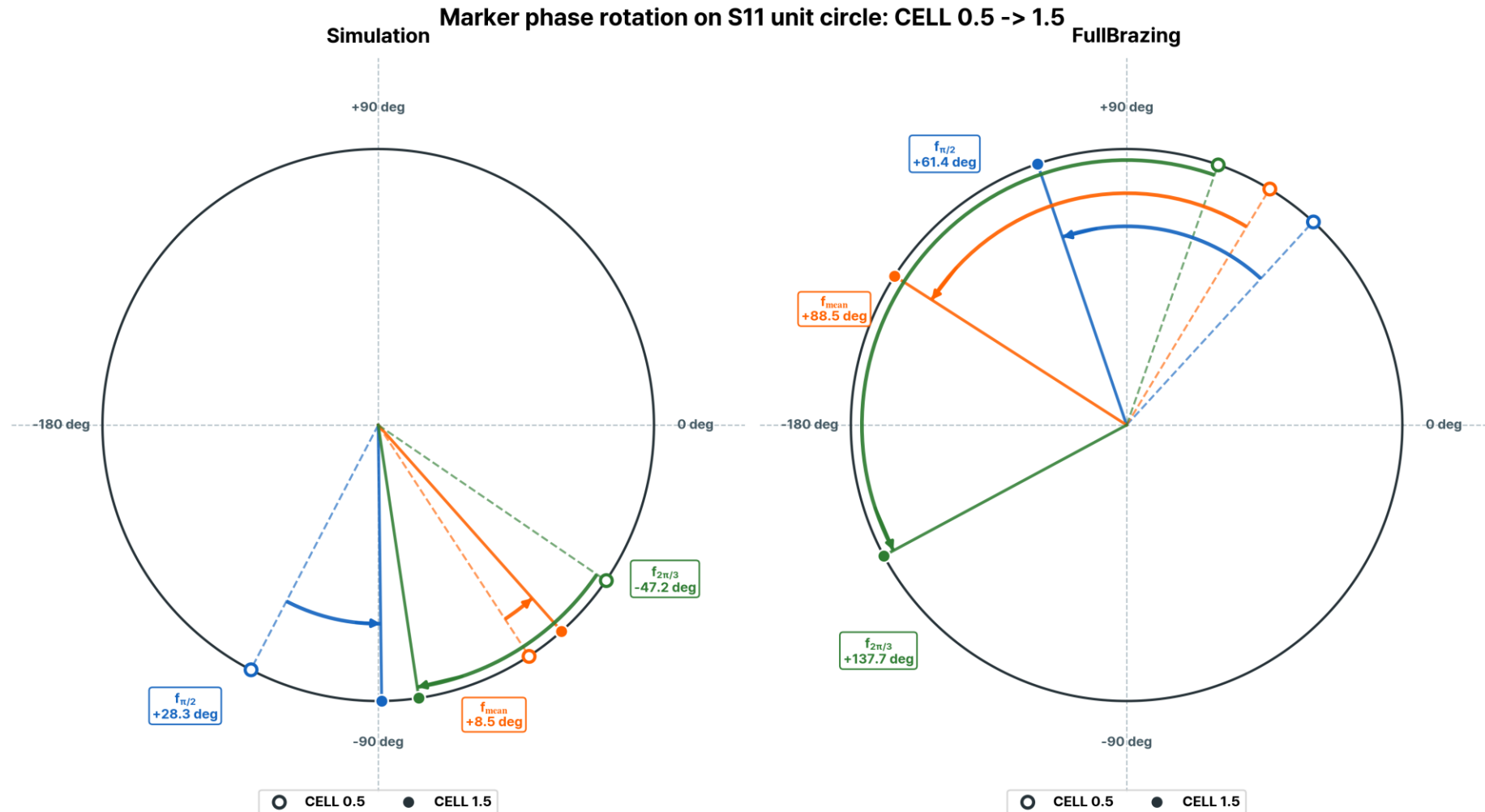
FullBrazing Marker phase on S11 unit circle: CELL 1.5



Method: kyhl method (Impedance matching method)

Frequency tuning based on the coupled-cell model.

Detune position desicion



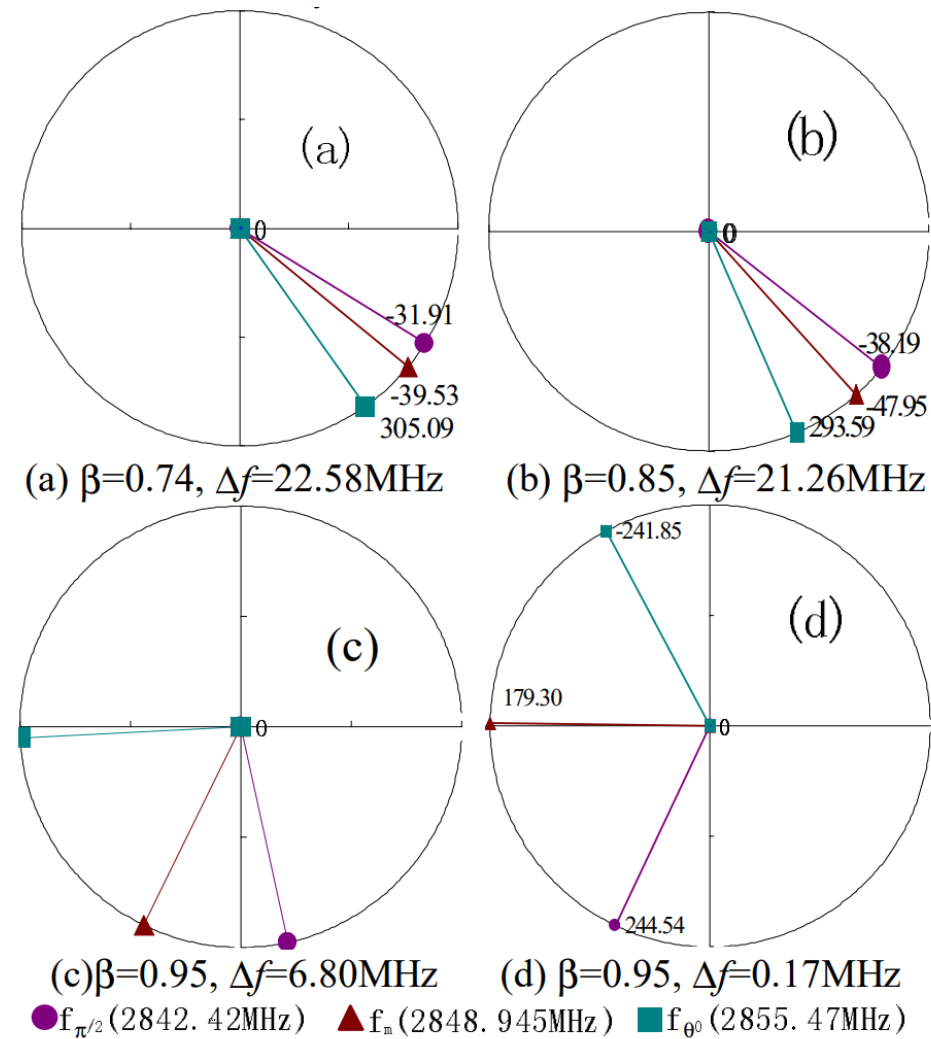


Figure 5. Example of one travelling wave accelerator coupler cavity tuning process

Next plan

Simulation: verify the simulation model

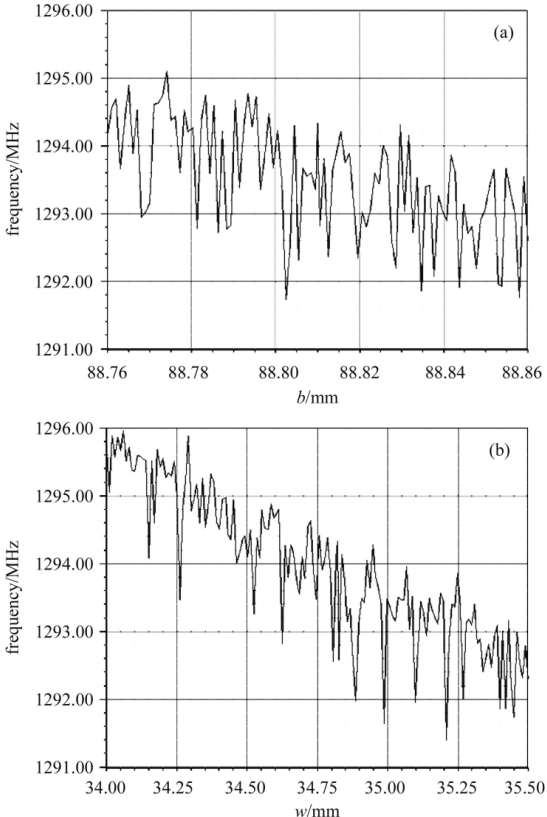


Fig. 5. The dependence of resonant frequency on coupler dimensions (a) b , (b) w when the first accelerating cavity is detuned with the plunger.

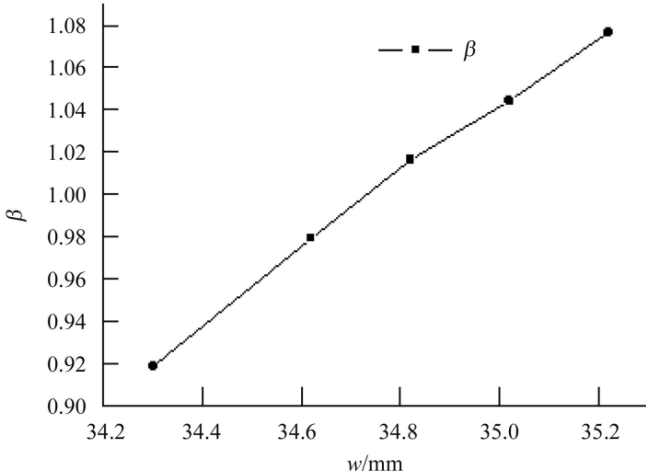


Fig. 6. The dependence of coupling coefficient on iris aperture.

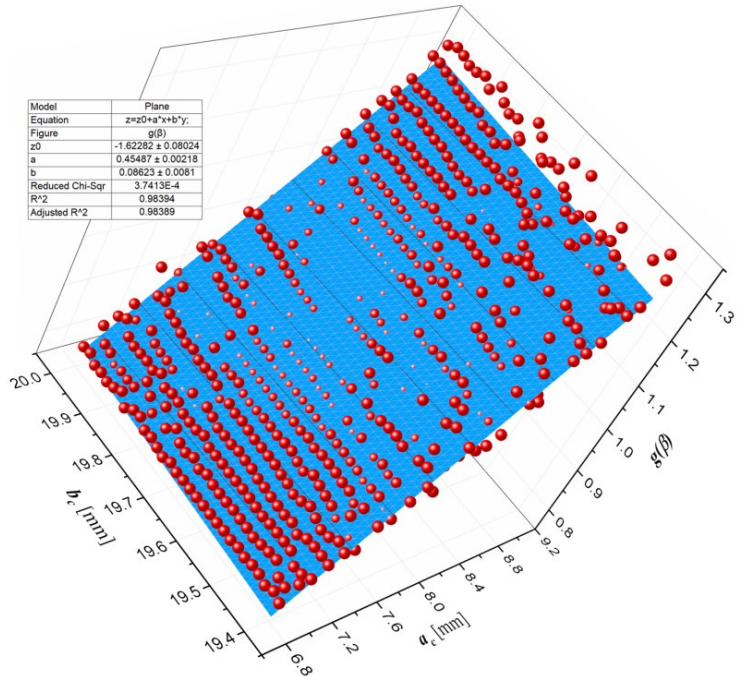


FIG. 6. $g(\beta)$ as a function of a_c and b_c . It is inserted with a linear fitting plane, and r^2 denotes the fitting accuracy between a simulated plane and a fitting plane.