

특론: 가속기 실험실습 I

(NUCE719P-01/PHYS715P-01, 정모세)

eLABs 시설을 이용한 빔운전 및 RF/빔진단 기초 2
(부제: RF 기초 1)

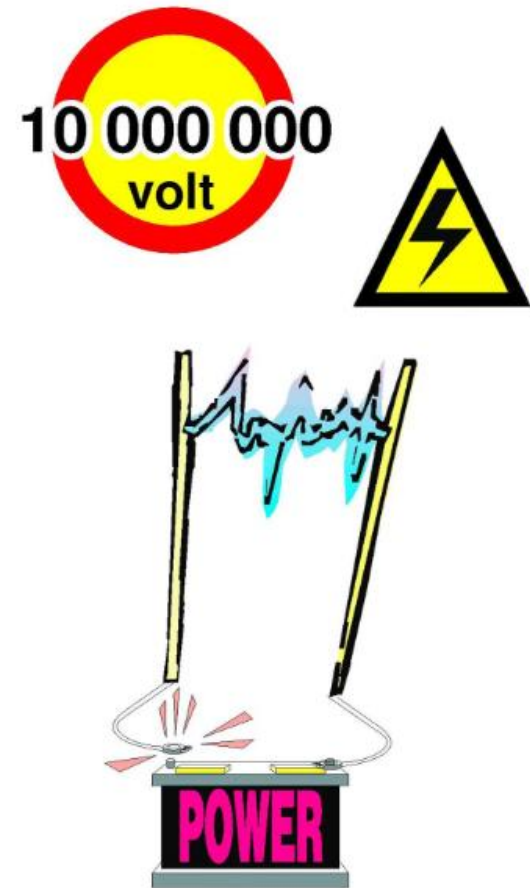
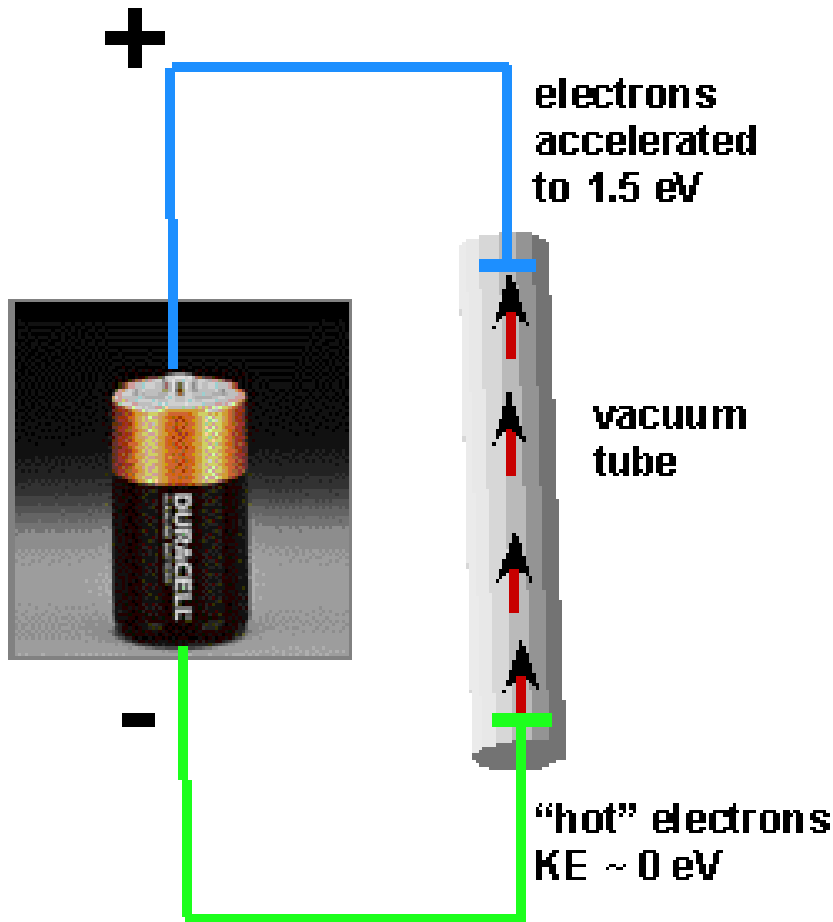
정모세

첨단원자력공학부 & 물리학과
moses@postech.ac.kr, 제1실험동 303호

- In general, charged particles are focused and bent by use of magnets, and **accelerated by use of electromagnetic waves in cavities.**

$$\mathbf{F} = q\mathbf{E} = q \left(-\nabla\phi - \frac{\partial\mathbf{A}}{\partial t} \right)$$

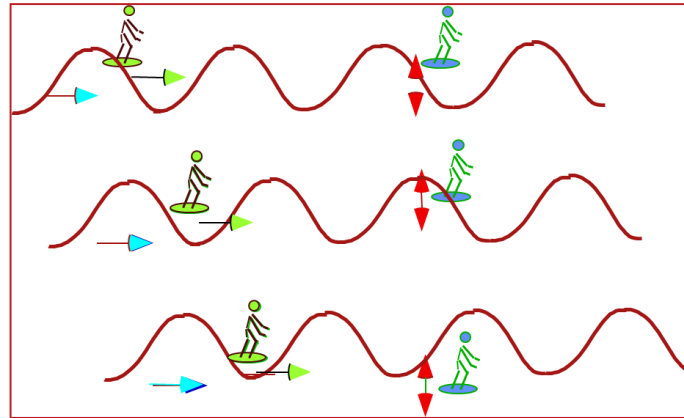
- DC acceleration is limited by high-voltage **sparking and breakdown**. It is very difficult to produce DC voltages more than **a few million volts**.
- RF accelerators bypass this limitation by applying **a harmonic time-varying electric field** to the beam, which is localized into bunches, such that the bunches always arrive when the field has the **correct polarity (phase)** for acceleration.
- The beam is accelerated within **electromagnetic-cavity structures**, in which a particular electromagnetic mode is excited from a high-frequency **external power source**.

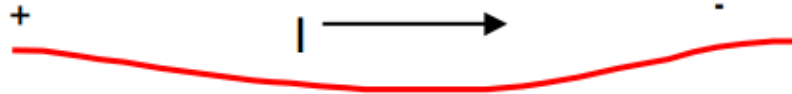


RF Acceleration

입자속도~파동속도

입자속도 << 파동속도





Low frequencies

- wavelengths \gg wire length
- current (I) travels down wires easily for efficient power transmission
- measured voltage and current not dependent on position along wire

펄스의 rise time 이 신호의
cable 통과 시간 보다 아주
느릴 때

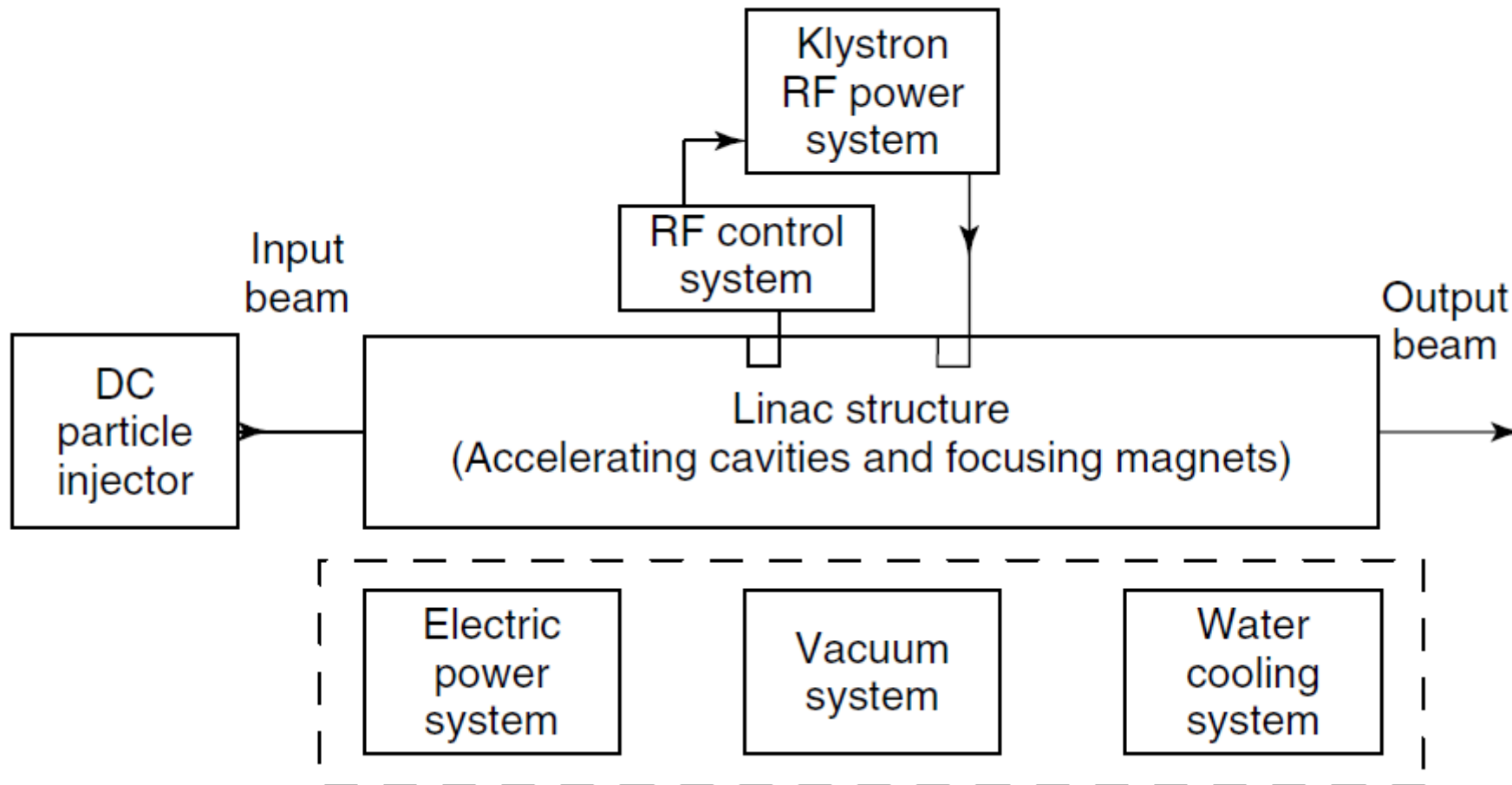
Freq.	Wavelength
60 Hz	5000 km
10 MHz	30 m
1 GHz	30 cm
40 GHz	7.5 mm
100 GHz	3 mm

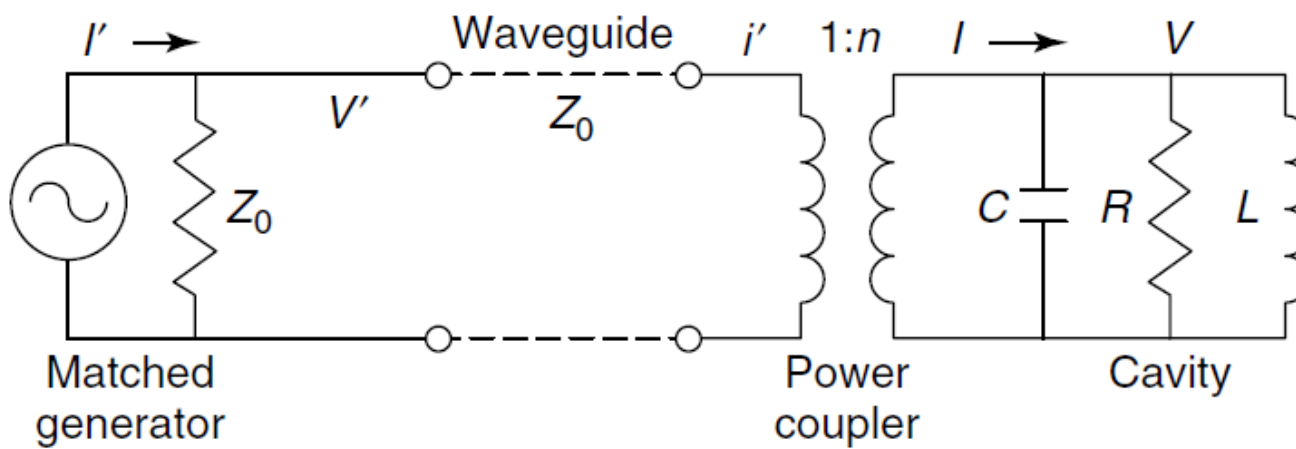
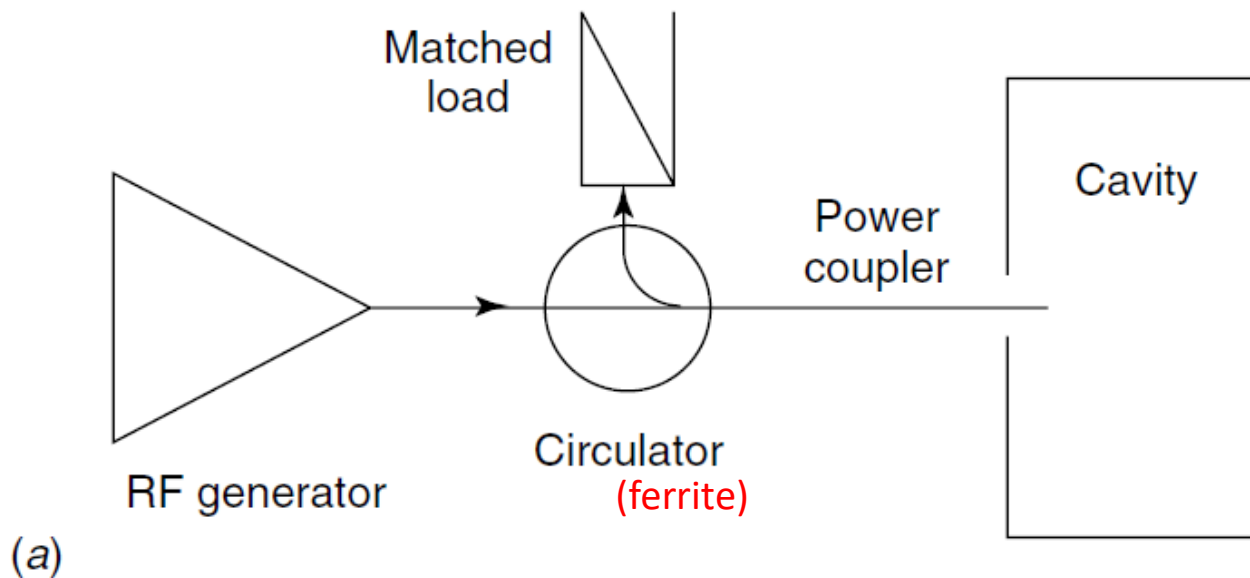


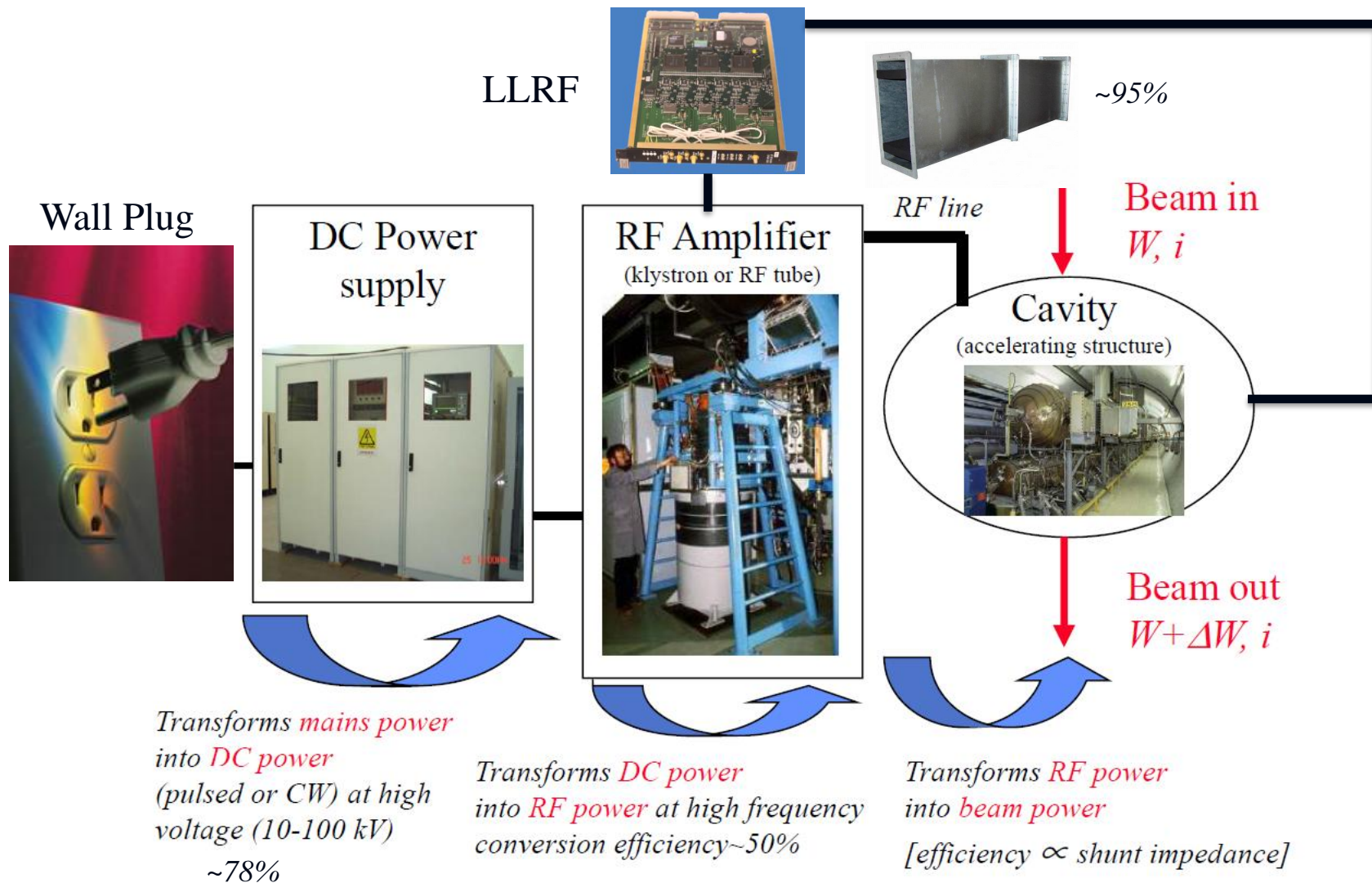
High frequencies

- wavelength \approx or \ll length of transmission medium
- need transmission lines for efficient power transmission
- matching to characteristic impedance (Z_0) is very important for low reflection and maximum power transfer
- measured envelope voltage dependent on position along line

펄스의 rise time 이 신호의
cable 통과 시간 보다 아주
빠를 때

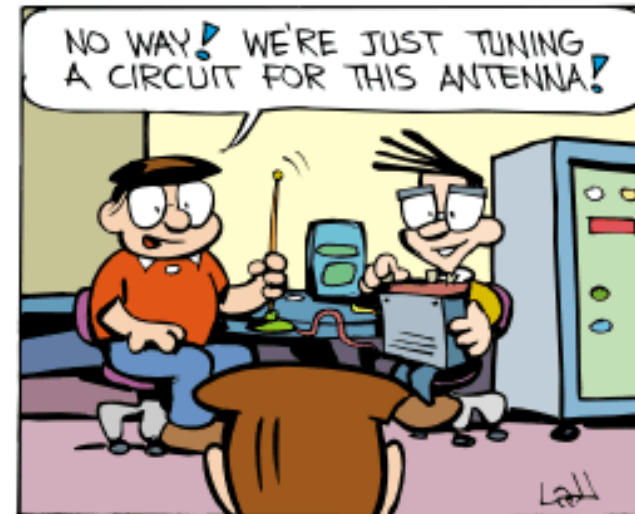
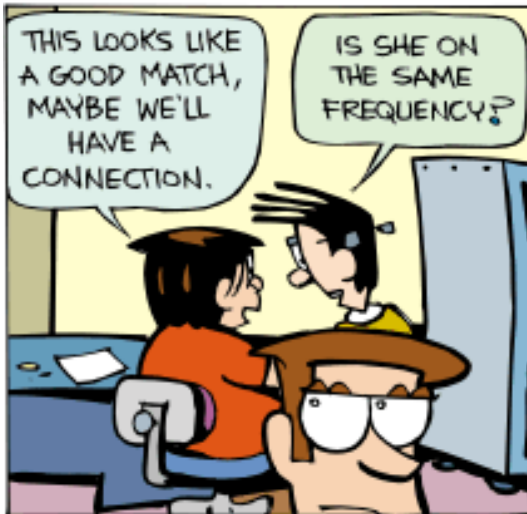






Building Blocks of RF Systems

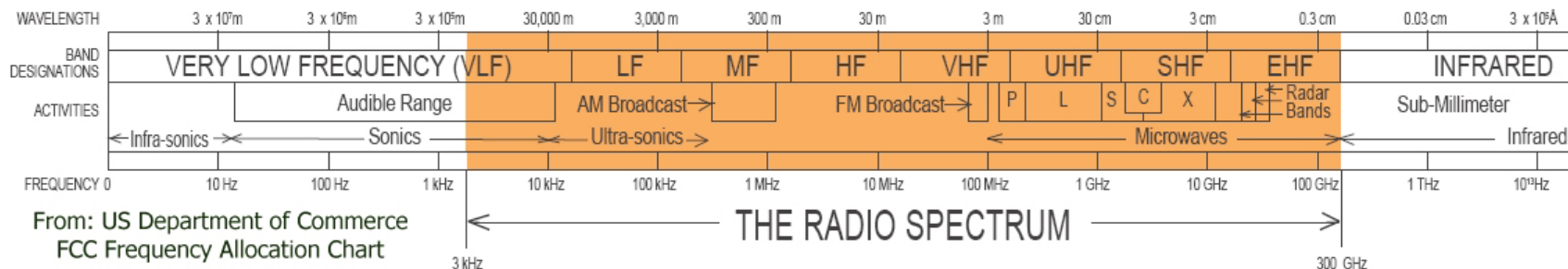
Return to Zero



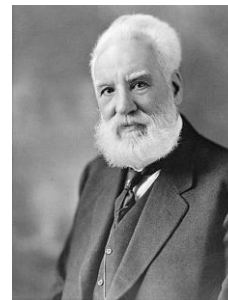
Hertz (Hz)



Heinrich Rudolf Hertz



IEEE Band	Frequency Range	Origin of Name	Wavelength in free space (centimeters)
L	1 to 2 GHz	L for "long" wave.	30.0 to 15.0
S	2 to 4 GHz	S for "short" wave	15 to 7.5
C	4 to 8 GHz	C for "compromise" between S and X band.	7.5 to 3.8
X	8 to 12 GHz	Used in WW II for fire control, X for cross (as in crosshair).	3.8 to 2.5
Ku	12 to 18 GHz	Ku for "kurz-under".	2.5 to 1.7
K	18 to 26 GHz	German "kurz" means short, yet another reference to short wavelength.	1.7 to 1.1
Ka	26 to 40 GHz	Ka for "kurz-above".	1.1 to 0.75
V	40 to 75 GHz	V for "very" high frequency band (not to be confused with VHF).	0.75 to 0.40
W	75 to 110 GHz	W follows V in the alphabet.	0.40 to 0.27



Alexander Graham Bell

- Means of expressing large values via a logarithmic ratio.

$$\text{dB} = 10 \times \log_{10} \left(\frac{P_2}{P_1} \right)$$

- In RF and microwave systems, typical power and voltage ratios are expressed in dB.

$$\text{dB} = 10 \times \log_{10} \left(\frac{V_2^2/R}{V_1^2/R} \right) = 20 \times \log_{10} \left(\frac{V_2}{V_1} \right)$$

- Sometimes, reference power is normalized to 1 mW.

$$\text{dBm} = 10 \times \log_{10} \left(\frac{P}{1 \text{ mW}} \right)$$

- Attenuation is

$$\text{Attenuation (dB)} = 10 \times \log_{10} \left(\frac{\text{Input power (W)}}{\text{Output power (W)}} \right)$$

dB	power ratio	amplitude ratio
100	10 000 000 000	100 000
90	1 000 000 000	31 623
80	100 000 000	10 000
70	10 000 000	3 162
60	1 000 000	1 000
50	100 000	316.2
40	10 000	100
30	1 000	31.62
20	100	10
10	10	3.162
6	3.981	1.995 (~2)
3	1.995 (~2)	1.413
1	1.259	1.122
0	1	1
-1	0.794	0.891
-3	0.501 (~1/2)	0.708
-6	0.251	0.501 (~1/2)
-10	0.1	0.316 2
-20	0.01	0.1
-30	0.001	0.031 62
-40	0.000 1	0.01
-50	0.000 01	0.003 162
-60	0.000 001	0.001
-70	0.000 000 1	0.000 316 2
-80	0.000 000 01	0.000 1
-90	0.000 000 001	0.000 031 62
-100	0.000 000 000 1	0.000 01

Typically supports frequencies up to **11 GHz**

Type N



APC 7



TNC



BNC



Typically supports up to **4 GHz**

SMA



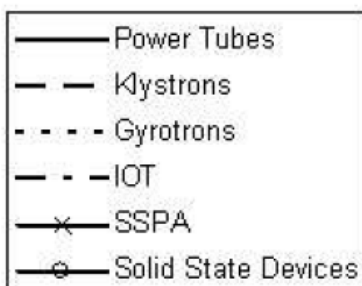
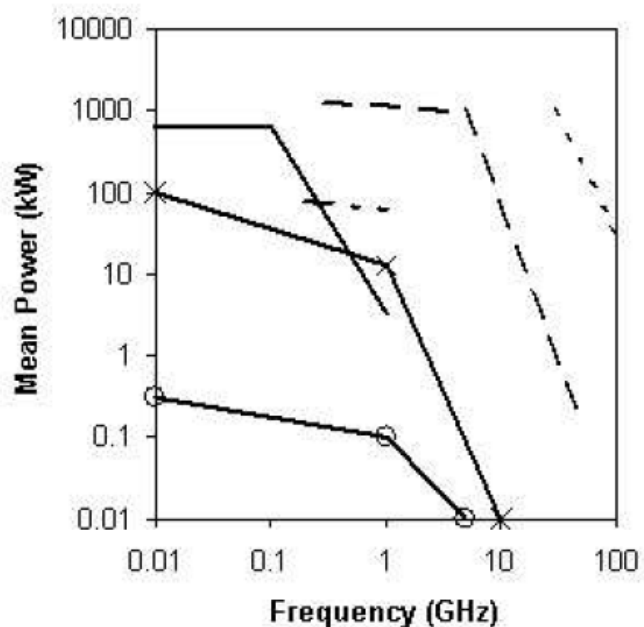
Connector used for high-frequency signal transmission
(Typically up to 18 GHz)

Lemo



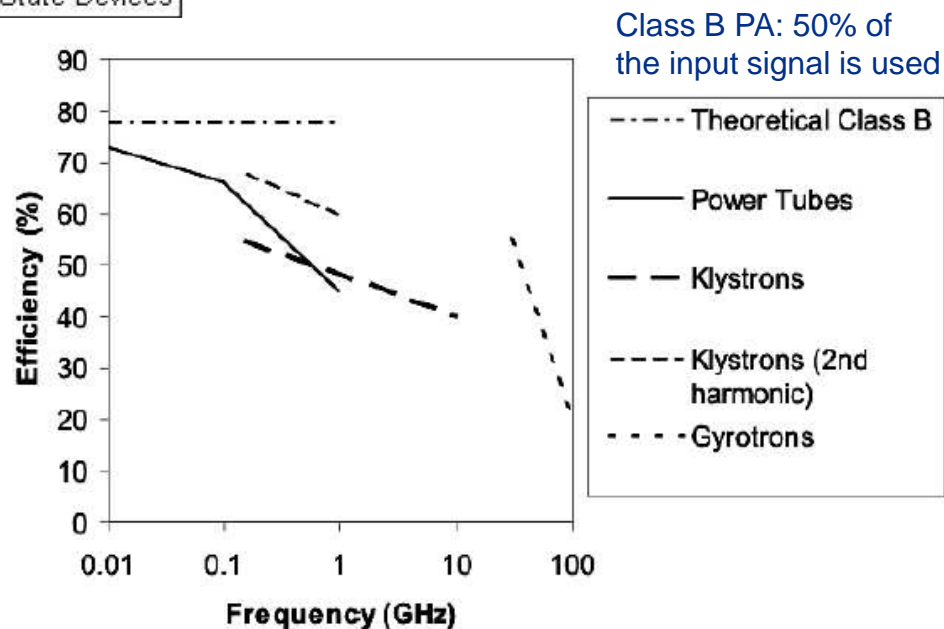
Ideal for compact applications
requiring high performance.

- The two main categories are **solid-state devices** and **vacuum tubes**.



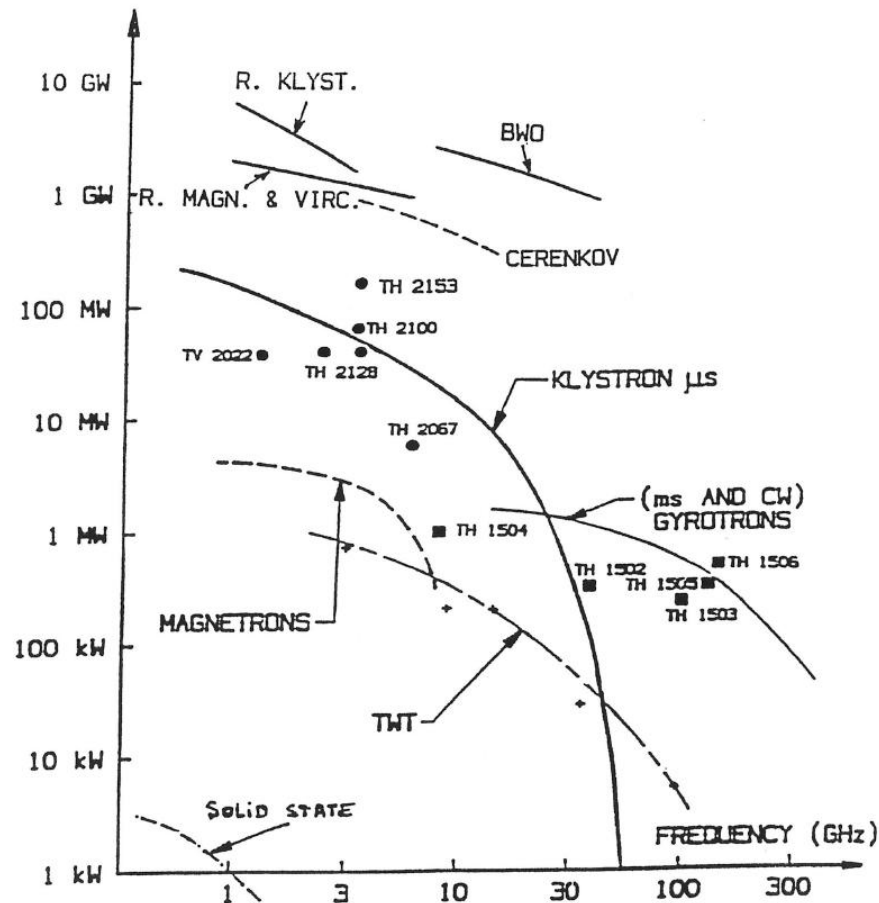
IOT: Inductive Output Tube

SSPA: Solid State Power Amplifier

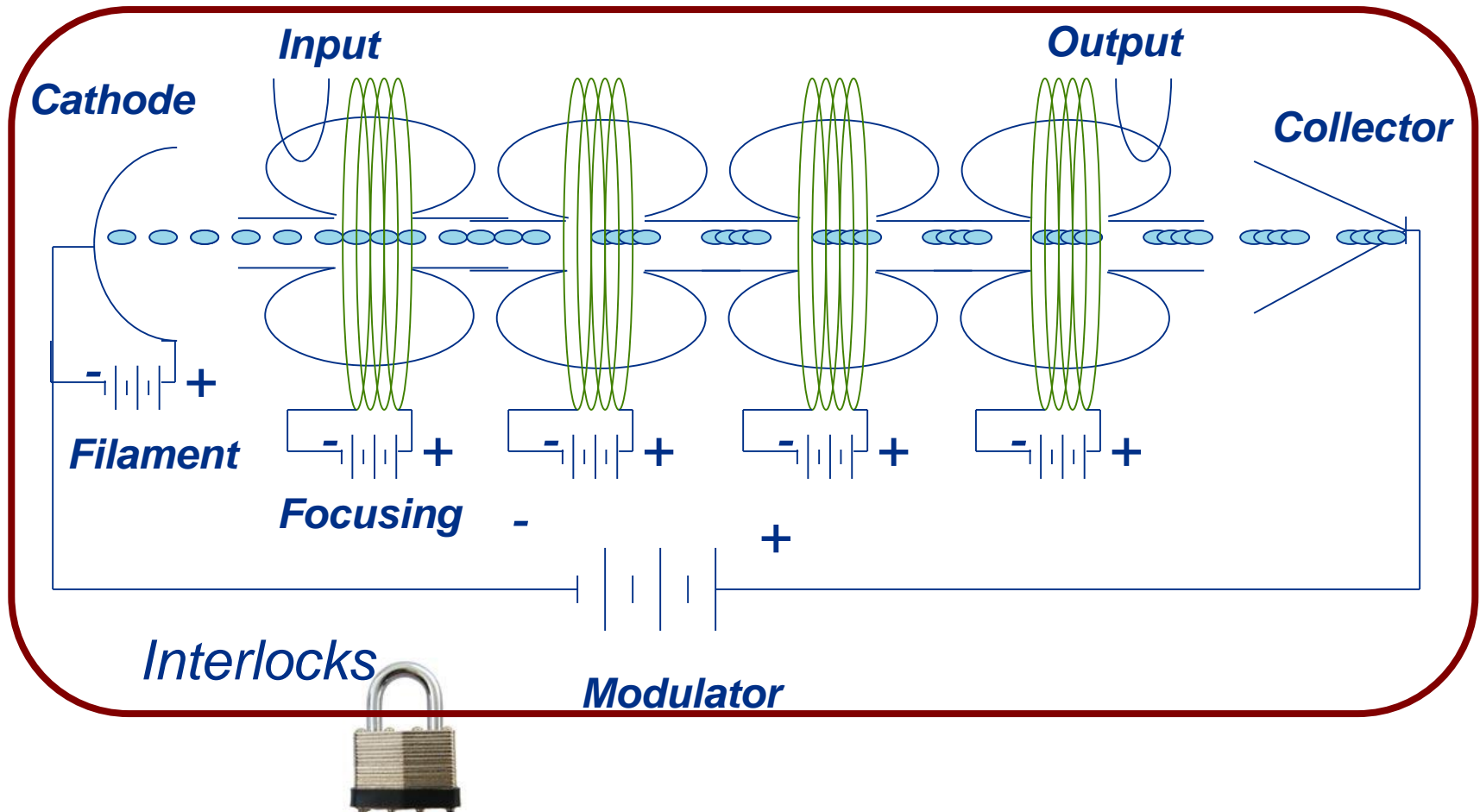


Class B PA: 50% of the input signal is used

- **Klystrons (>350 MHz)** for electron linacs and modern proton linacs. RF distribution via waveguides.
- **RF tube (<400 MHz) or solid state amplifiers** for proton and heavy ion linacs. RF distribution via coaxial lines.



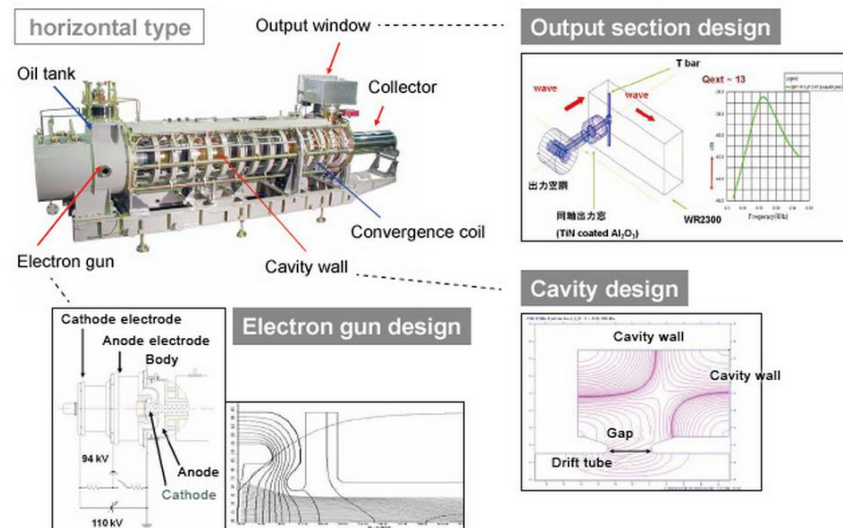
- Decelerator: Amplify RF signals by **converting the kinetic energy** in a DC electron beam into radio frequency power. (velocity modulation \rightarrow bunching)



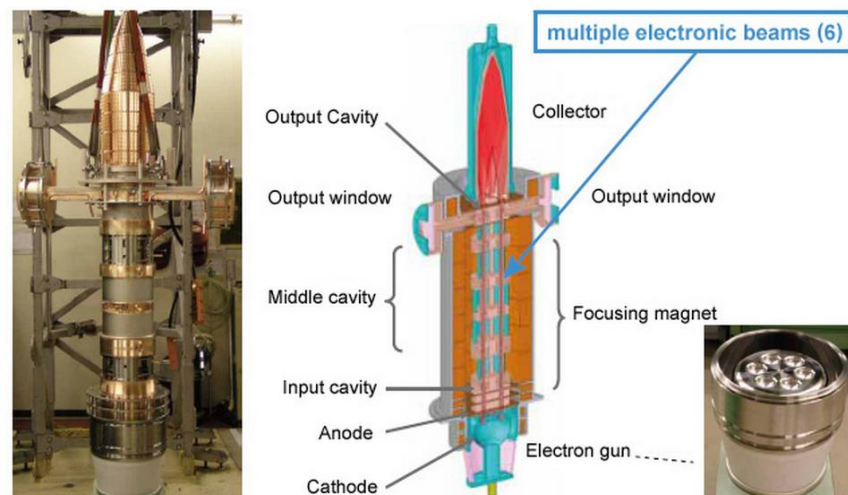
Typical Klystron Parameters



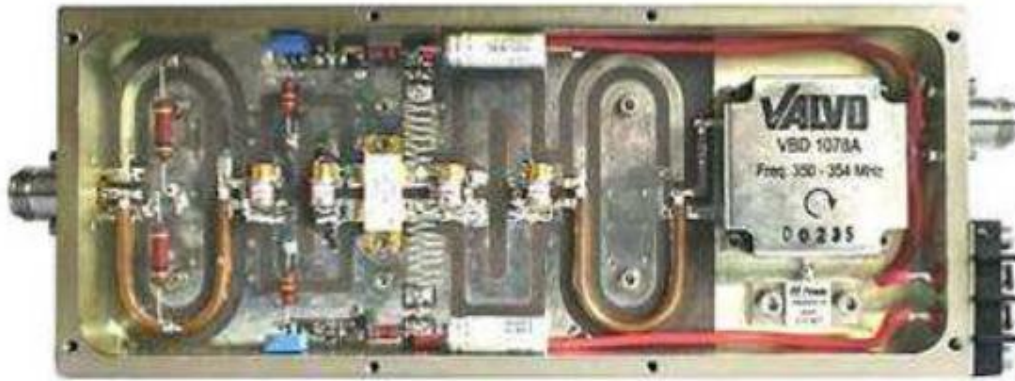
- Power Gain 40-60 dB (10^4 - 10^6)
- Power 10^3 to 10^7 Watts
- Duty Cycle Continuous or Pulsed
- Frequency Hundreds MHz to Tens GHz
- Bandwidth 1%
- Efficiency 50%
- Cathode Volts 10' s to 100' s of kilovolts
- Klystron Life 10,000-100,000 hours



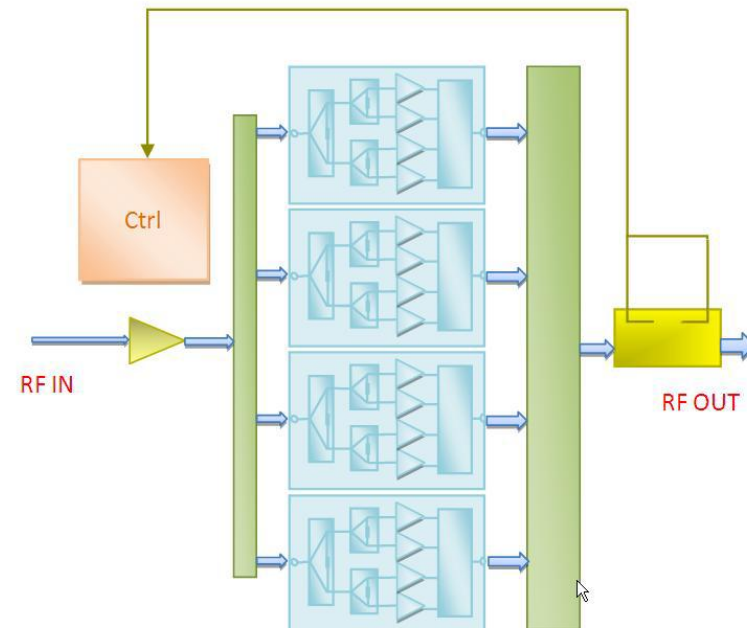
Toshiba



- Solid state amplifiers are **based on transistors** instead of vacuum electron tubes as active device.



- 330 W module
- 352 or 500 MHz, different devices
- 1 transistor/pallet
- 1 circulator/transistor
- © Synchrotron SOLEIL - Ti Ruan



Typical Solid State Parameters



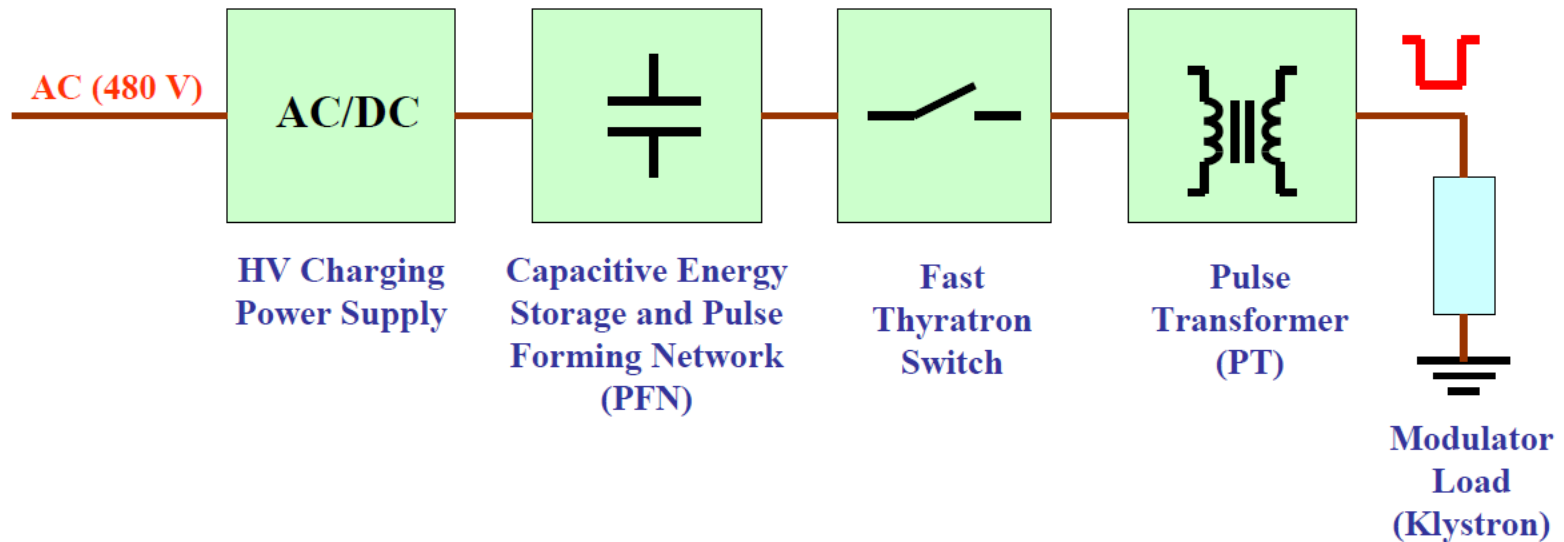
- Power Gain 20-70 dB (10^2 - 10^7)
- Power 10^3 to 10^5 Watts
- Duty Cycle Continuous or Pulsed
- Frequency 1 MHz to 2 GHz
- Bandwidth few % to decades %
- Efficiency 10-50%
- Supply Volts **20-50 volts DC**
- Life time 10,000-200,000 hours



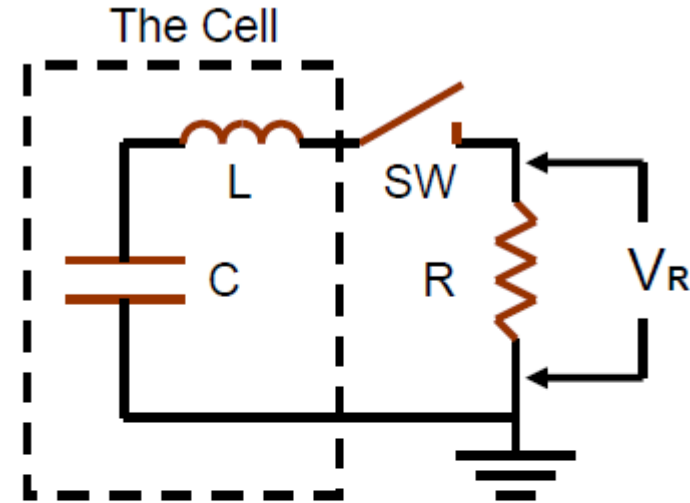
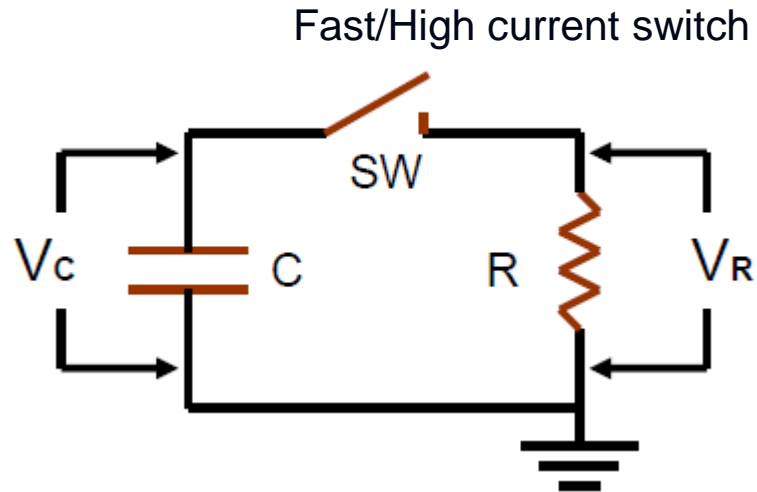
Bruker



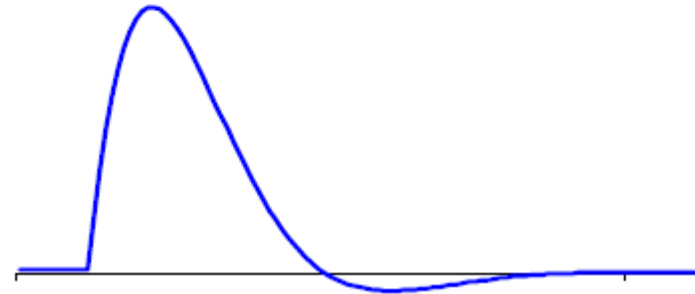
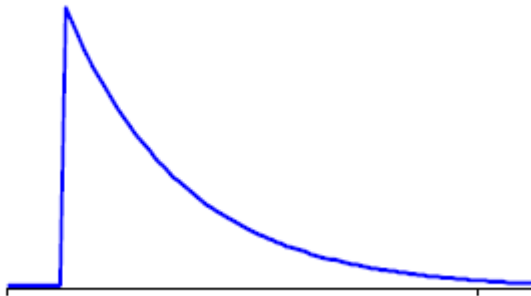
- The modulators are locally and remotely controlled **pulse generators** that supply high-voltage pulses required for proper operation of **high-power pulsed RF amplifiers**.

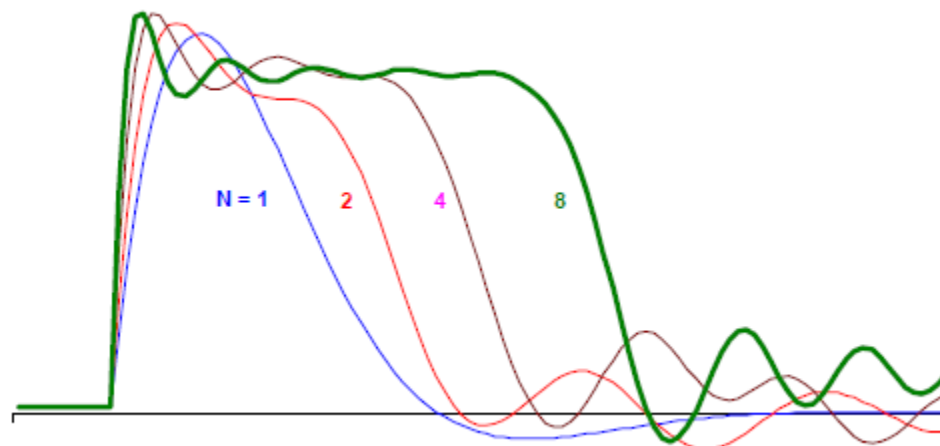
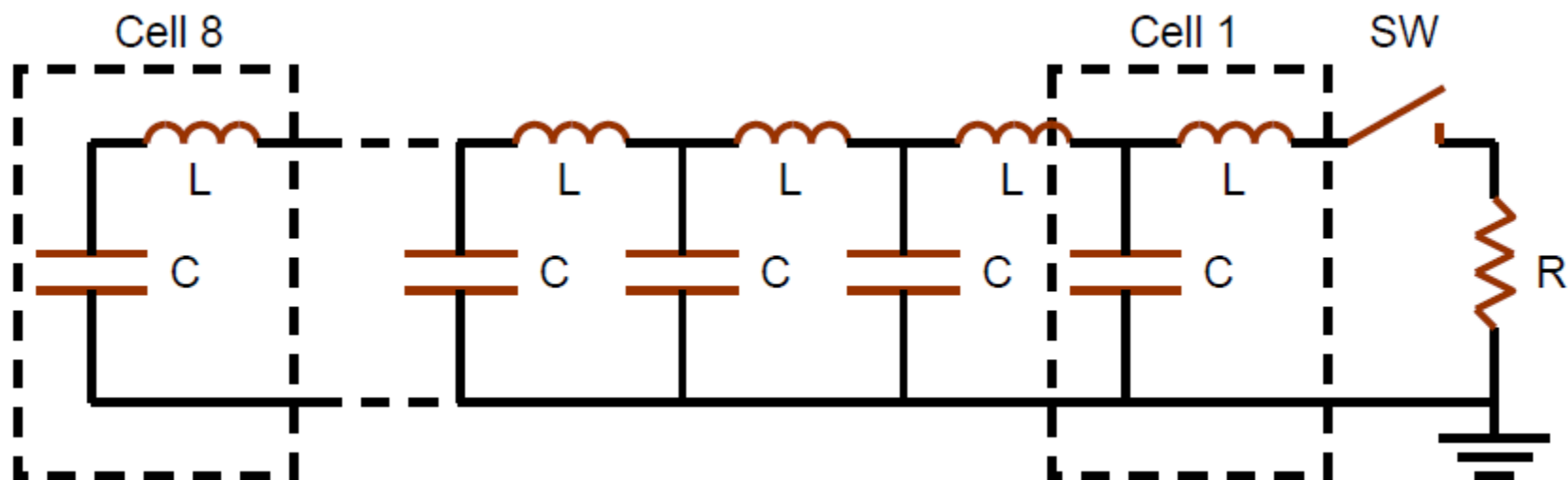


Pulse Forming

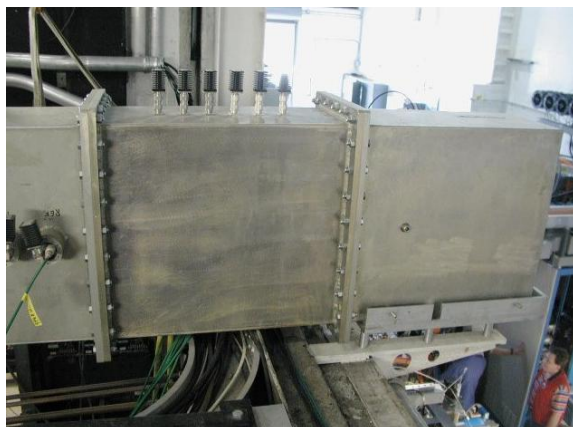
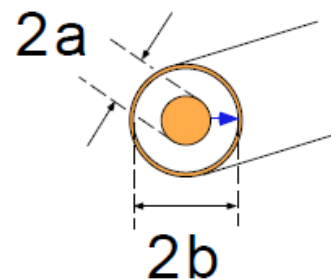
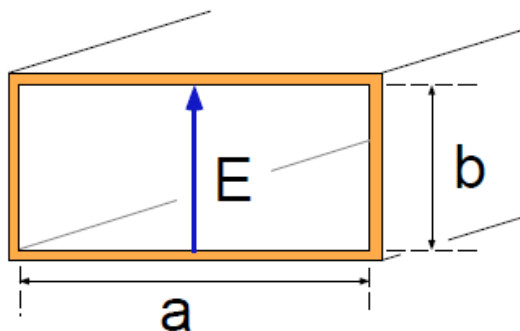


Fast/High current switch





- Transmission lines transmit RF power from one point to another with **minimum loss and external radiation of energy**.
- Two common types: Rectangular waveguide type / Coaxial type



Rigid line

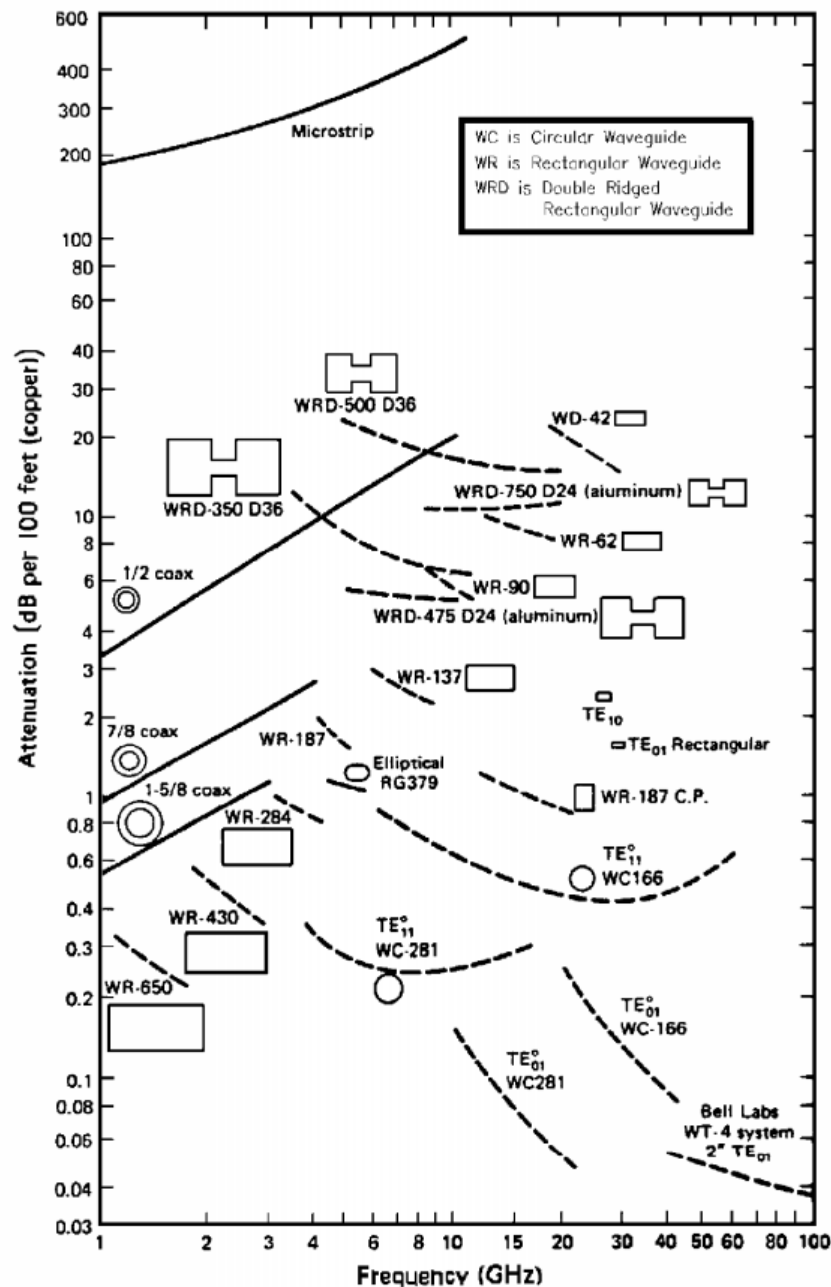


Hard line (Heliax)

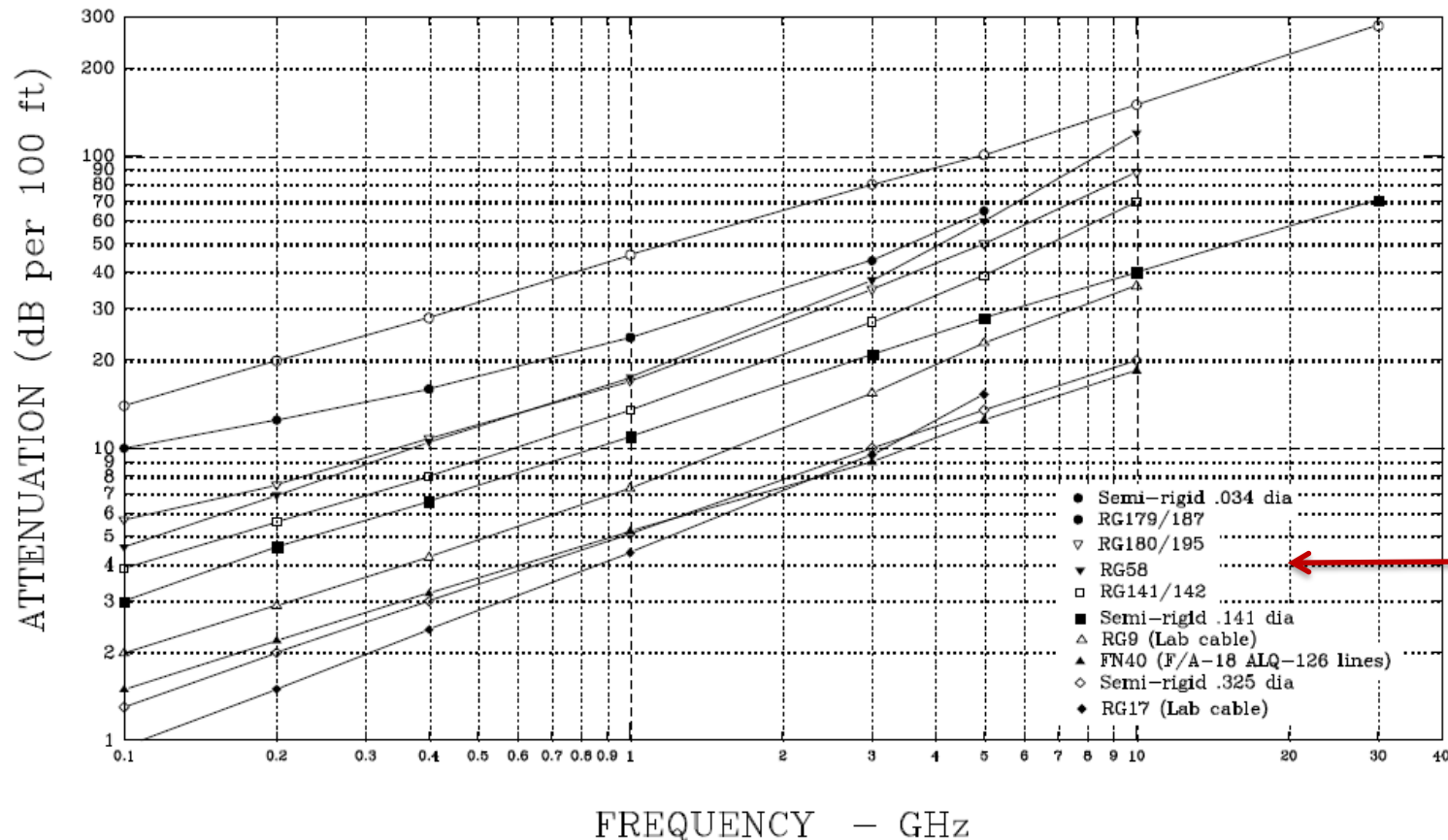
- Commonly used rectangular waveguides have an aspect ratio b/a of ~ 0.5 .



6.50"



- Coaxial cable is used for frequencies up to about **400 MHz** and down to DC and waveguide at higher frequencies, where the loss is less than coaxial cable.





- Typically, a coaxial cable will have a dielectric with relative dielectric constant ϵ_r between the inner and outer conductor, where $\epsilon_r = 1$ for vacuum, and $\epsilon_r = 2.29$ for a typical polyethylene-insulated cable.

$$Z_0 = \frac{1}{\sqrt{\epsilon_r}} 60 \ln \left(\frac{b}{a} \right) \qquad v_{ph} = \frac{c}{\sqrt{\epsilon_r}}$$

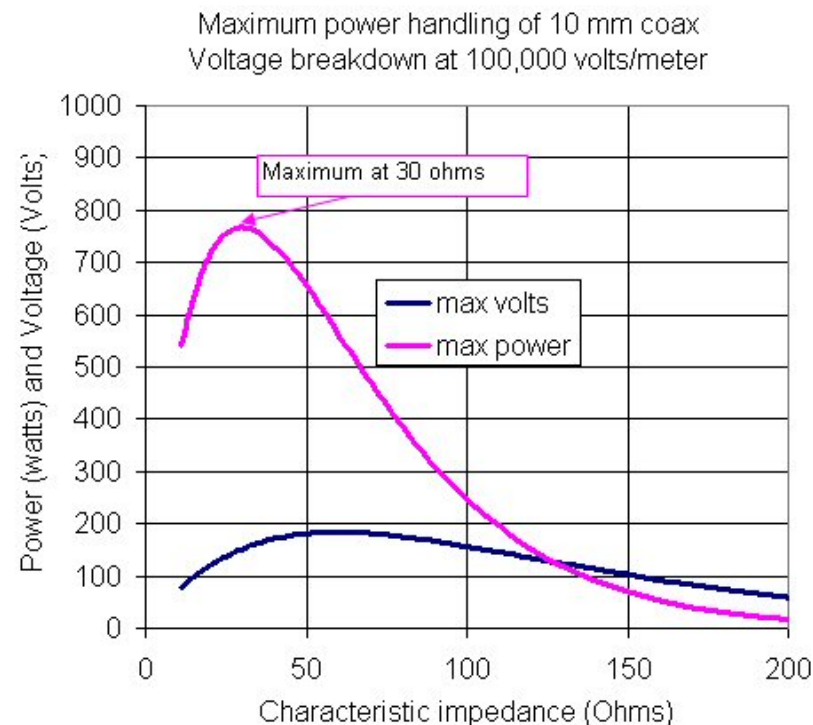
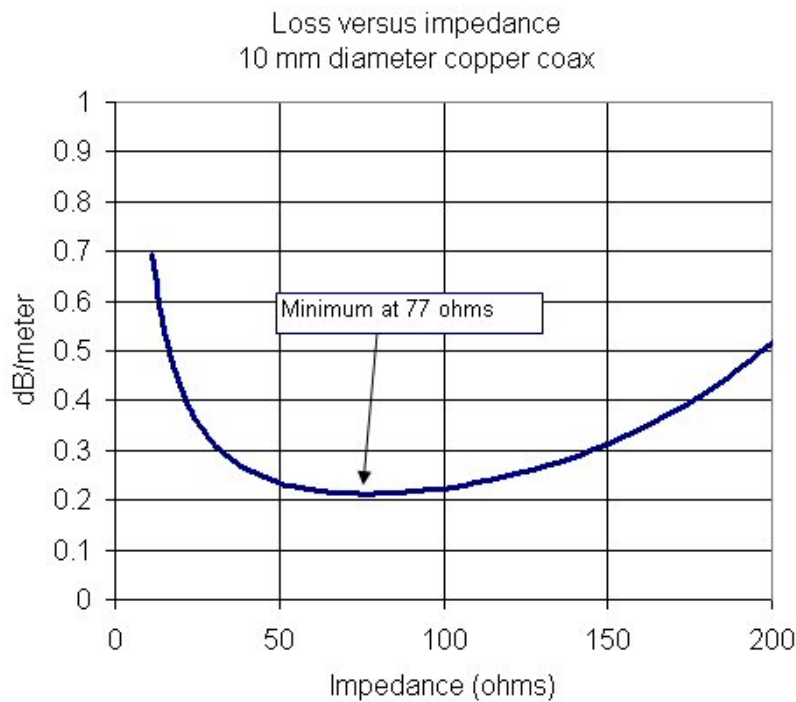
- For a polyethylene-insulated coaxial cable, the propagation velocity is **roughly 2/3 the speed of light**:

$$v_{ph} = 0.66c$$

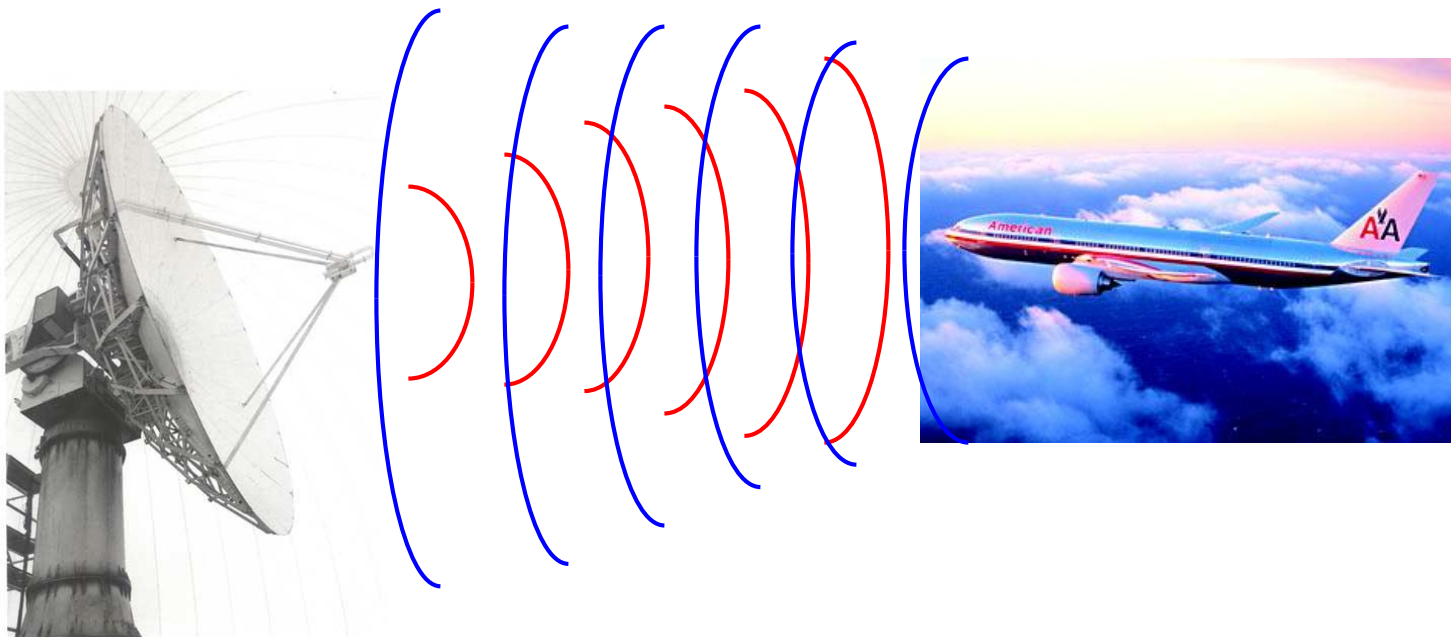
Ex] 1 nsec time delay in RG58 cable: ~ 19.8 cm

Why 50 Ohms ?

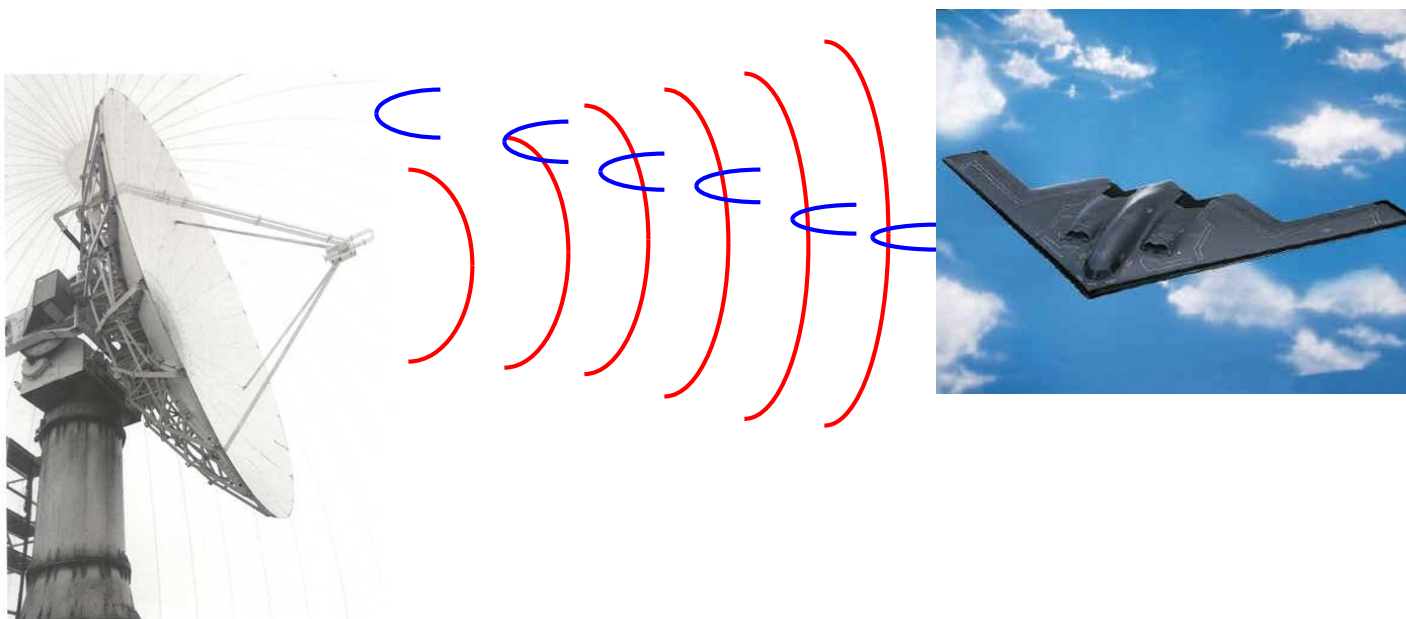
- The arithmetic mean between 30 ohms (best power handling) and 77 ohms (lowest loss) is 53.5, the geometric mean is 48 ohms. Thus the choice of 50 ohms is **a compromise between power handling capability and signal loss per unit length**, for air dielectric.



Impedance Matching

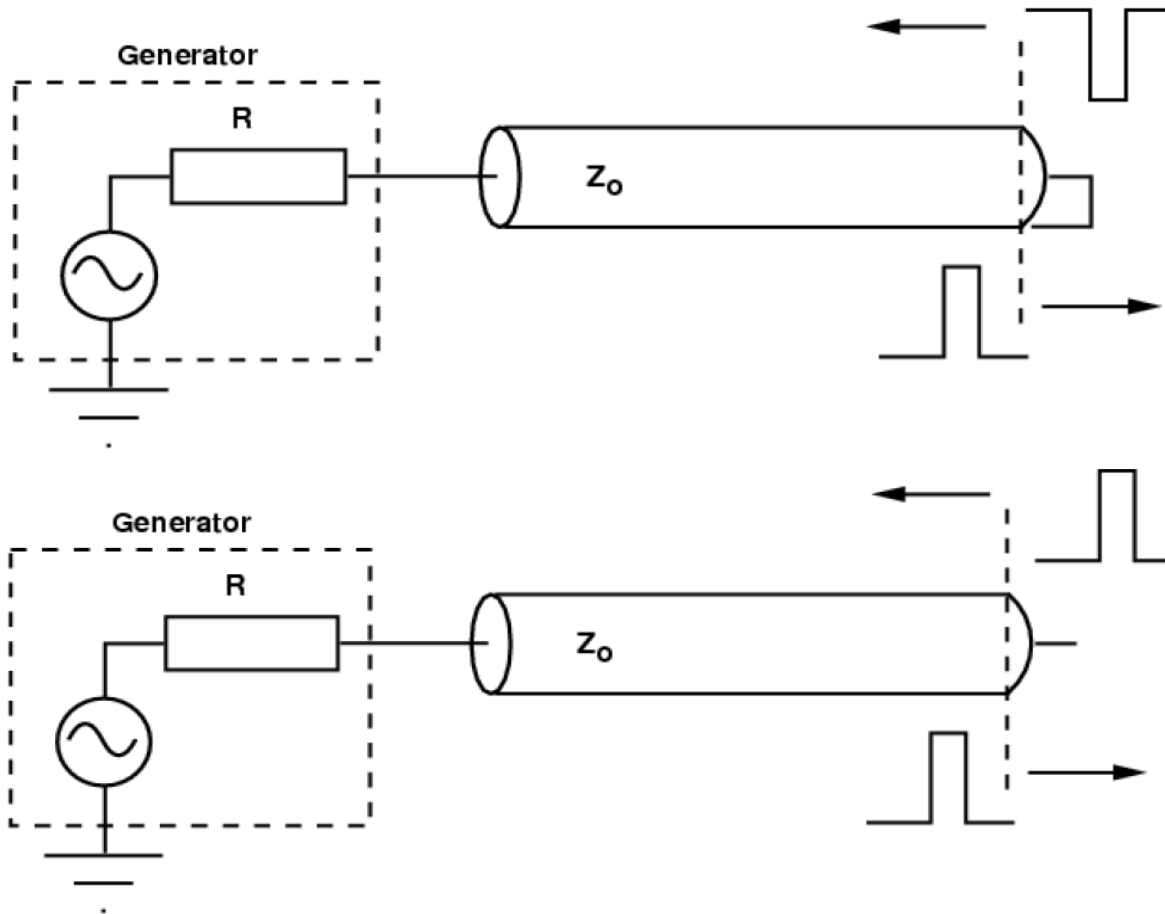


Radar works due to poor matching



Better matching (absorption) with the Stealth !

- Note that the generator has an internal impedance R . If $R = Z_0$, the returning pulse is completely absorbed in the generator (**Matched generator**).



Short ($Z_L = 0$)

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{\beta_c - 1}{\beta_c + 1}$$

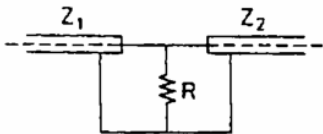
Open ($Z_L \rightarrow \infty$)

Example 13.1 A signal is to be sent from a coaxial cable of impedance Z_1 into another coaxial cable of impedance Z_2 . What termination scheme should be used in order to avoid reflections?

Two cases arise:

a) $Z_1 < Z_2$

Here the impedance which cable 1 sees must be reduced. This implies adding a resistance R in parallel to cable 2, i.e.,



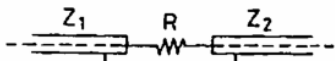
Since the combination must equal Z_1 we find

$$\frac{RZ_2}{R + Z_2} = Z_1$$

$$R = \frac{Z_1 Z_2}{Z_2 - Z_1}$$

b) $Z_1 > Z_2$

Since the impedance seen by cable 1 must be increased, we add a resistance R in series.



Then,

$$Z_2 + R = Z_1 \Rightarrow R = Z_1 - Z_2$$

Some other possible situations which often arise are summarized in Table 13.2 along with the termination scheme to be used.

Table 13.2. Cable termination schemes

Cable impedance = Z_c		
Source	Load	Termination scheme
$Z_s = Z_c$	$Z_L = Z_c$	No termination necessary
$Z_s = Z_c$	$Z_L > Z_c$	Receiving end; parallel $R = Z_c / (1 - Z_c / Z_L)$
$Z_s = Z_c$	$Z_L < Z_c$	Receiving end; series $R = Z_c - Z_L$
$Z_s < Z_c$	$Z_L = Z_c$	Sending end; series $R = Z_c - Z_s$
$Z_s > Z_c$	$Z_L = Z_c$	Sending end; parallel $R = Z_c / (1 - Z_c / Z_s)$
Combinations of the above situations may also arise in which case an appropriate combination of termination schemes may be used, e.g.,		
$Z_s < Z_c$	$Z_L > Z_c$	Receiving end; parallel $R = Z_c / (1 - Z_c / Z_L)$ with sending end; series $R = Z_c - Z_s$



Directional Coupler



Three Stub Tuners

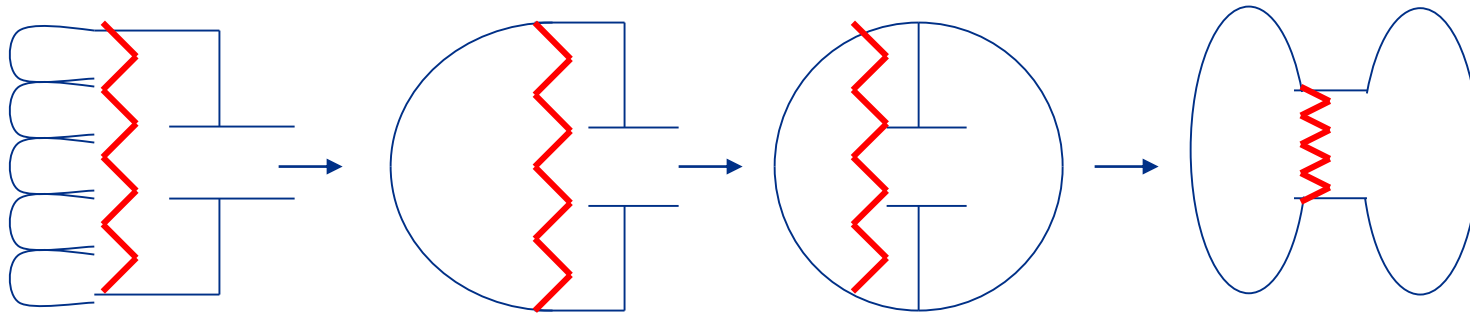


Circulator/Isolator

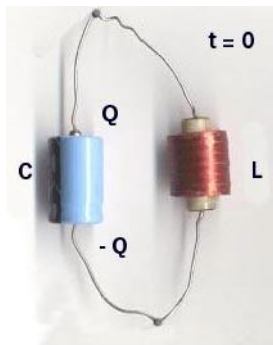


Waveguide Load

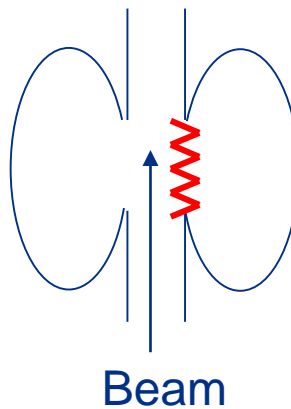
LC Circuit to RF Cavity



Shunt
Impedance



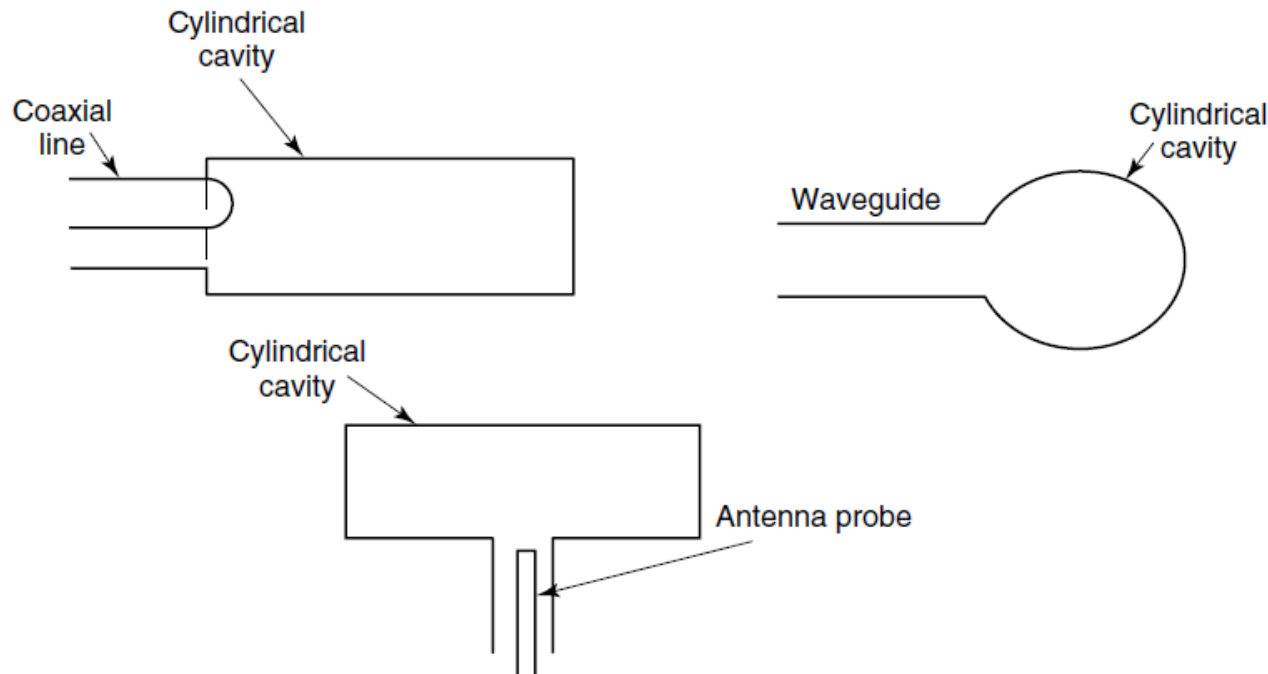
$$\omega = 2\pi f = \frac{1}{\sqrt{LC}}$$



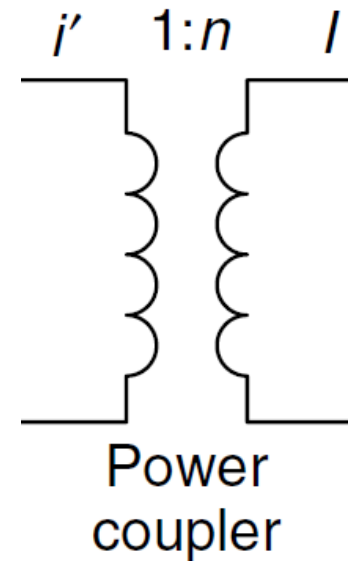
$$r_s = \frac{V_0^2}{P}$$

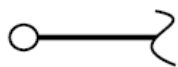
Effectiveness of
producing an axial
voltage for a given
power dissipated

- The coupling mechanism and the waveguide are represented by a transformer with a turns ratio of 1: n .



$$\frac{V'}{V} = \frac{i}{i'} = \frac{1}{n}$$

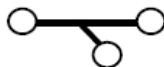




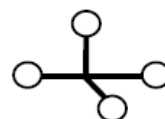
load



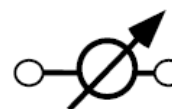
**directional
coupler**



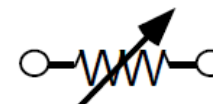
tee



**magic
tee**



phase-shifter



**variable
attenuator**



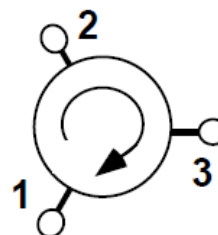
**low-pass
filter**



**high-pass
filter**



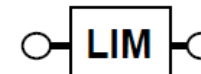
**band-pass
filter**



circulator



isolator
protect RF components
from reflected signals
(passive)

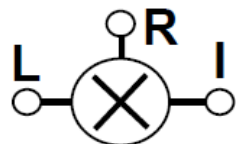


limiter
prevents excessive
power levels

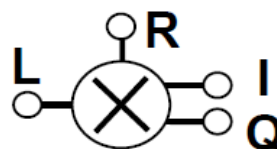


diode

an active
semiconductor device
to process RF signals



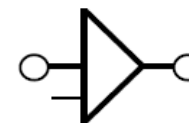
mixer



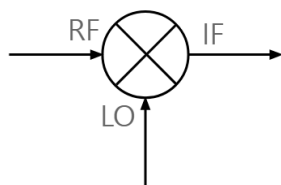
IQ mixer



oscillator



amplifier



Time vs Frequency

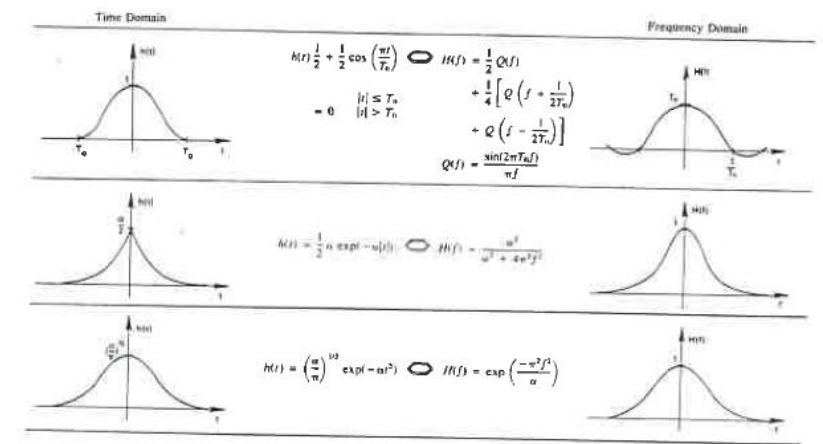
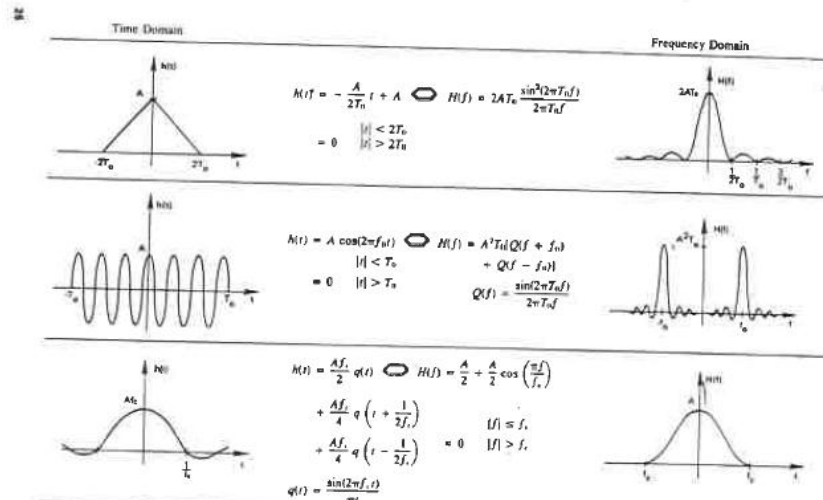
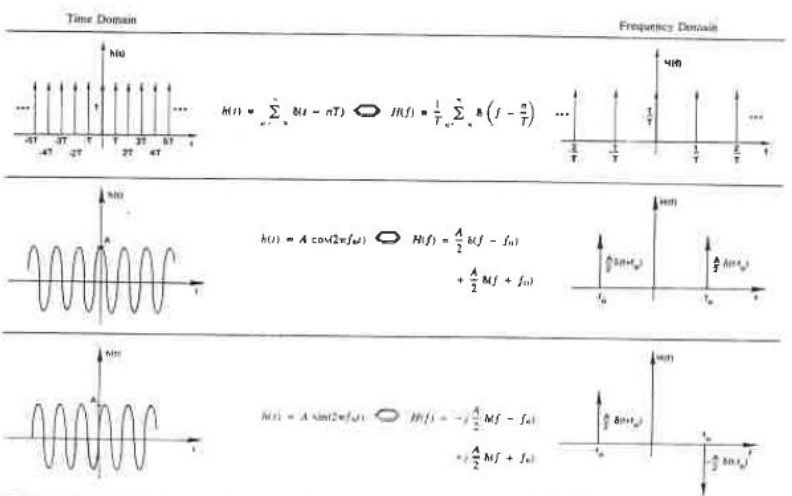
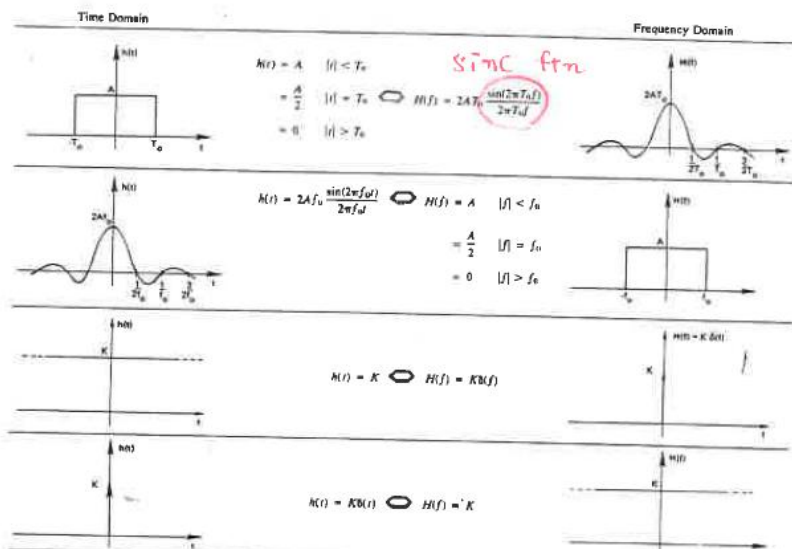


Figure 2.12 (cont.)

여기는 time convolution

Sec. 4.5 Time-Convolution Theorem

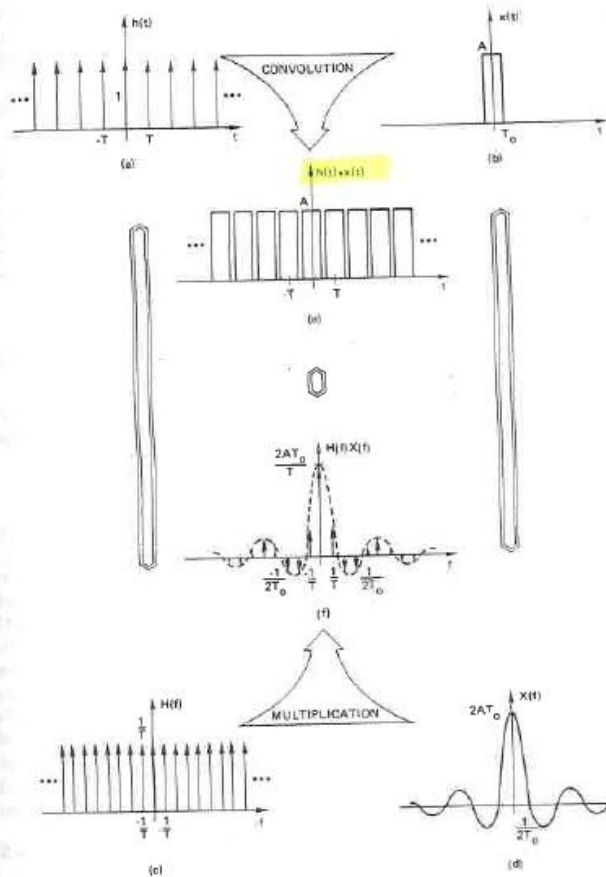


Figure 4.10 Example application of the convolution theorem.

이제는 freq. convolution

4.6 FREQUENCY-CONVOLUTION THEOREM

We can equivalently go from convolution in the frequency domain to multiplication in the time domain by using the frequency-convolution theorem: the Fourier transform of the product $h(t)x(t)$ is equal to the convolution $H(f)$

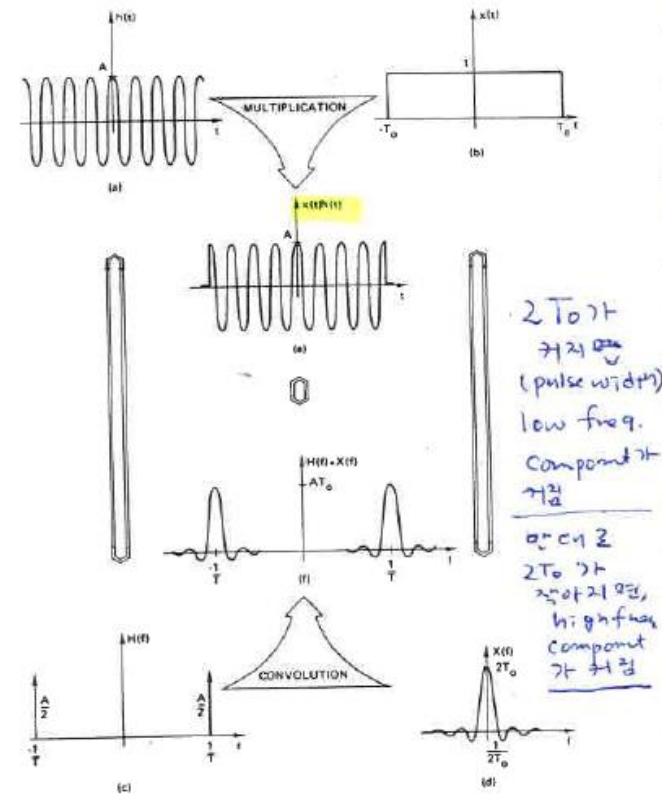
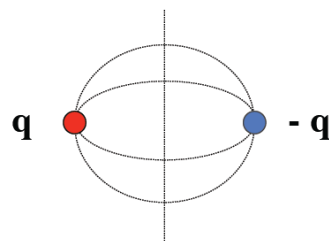
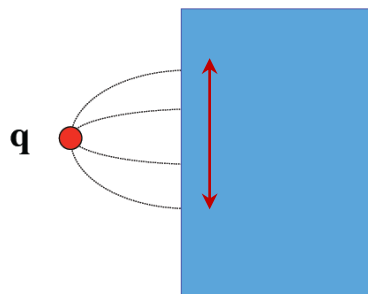


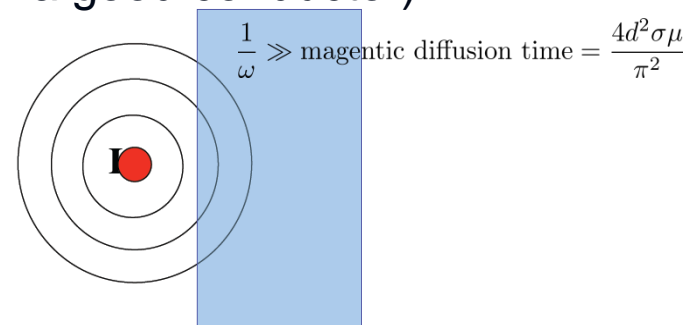
Figure 4.11 Graphical example of the frequency-convolution theorem.

Boundary Conditions

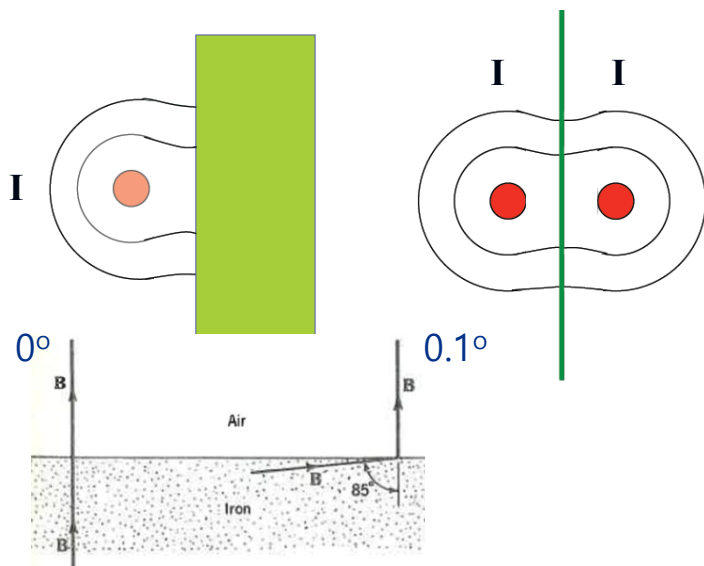
- Electric field near a good conductor:



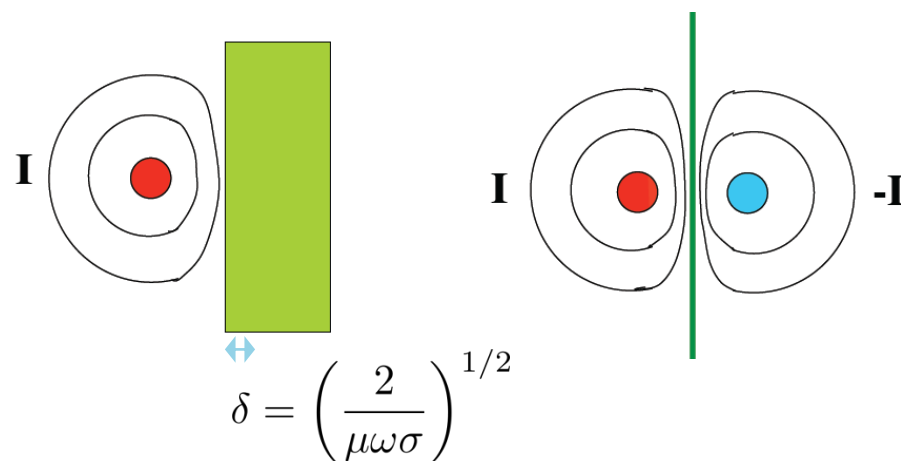
- Static magnetic field near $\mu_r \approx 1$ (even in the case of a good conductor)



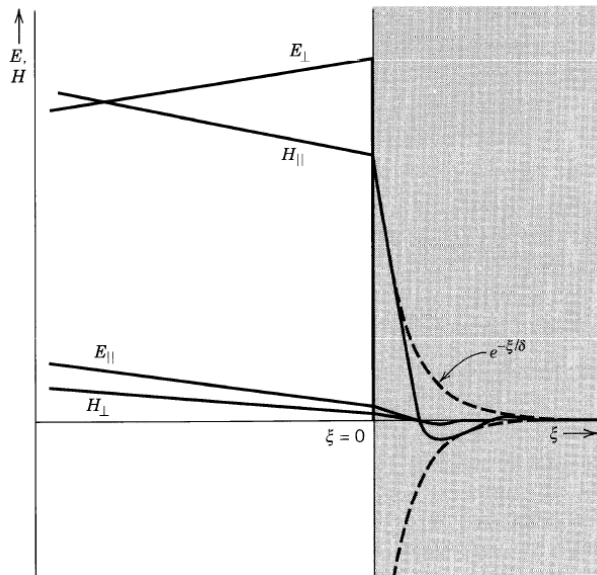
- Static magnetic field near $\mu_r \gg 1$ (i.e., ferromagnetic material)



- Time-varying magnetic field near a good conductor (i.e., small skin depth):

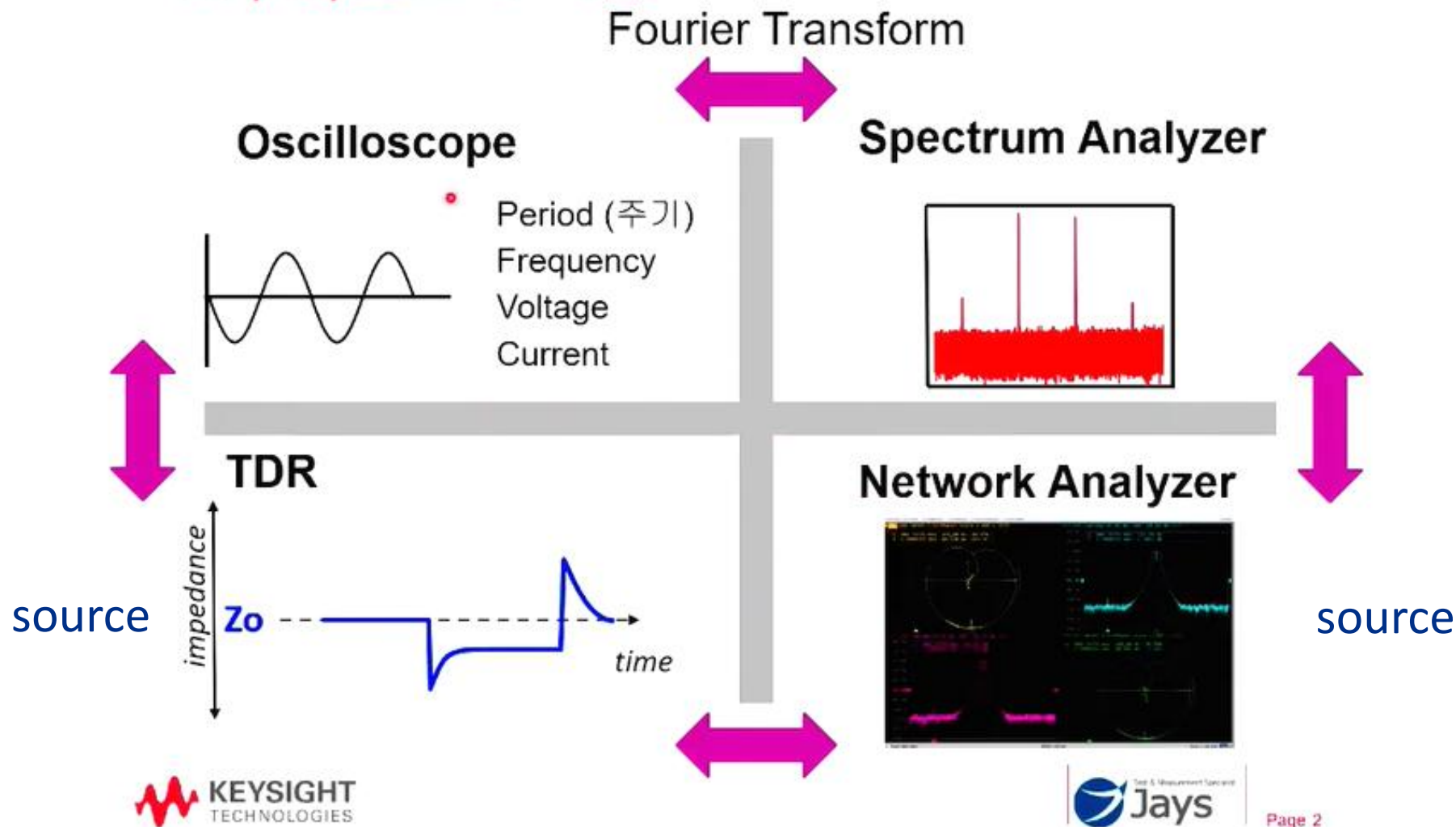


We commonly classify the solutions to the wave equation in the following types:



- 1) TEM modes
Waves that contain neither electric nor magnetic field in the direction of propagation. The name transverse electromagnetic mode arises from the fact that all of the fields lie entirely in the transverse plane. They are the usual transmission line waves along a multiconductor guide.
- 2) TM modes
Waves that contain electric field but no magnetic field in the direction of propagation. Also known as E, or electric, waves.
- 3) TE modes
Waves that contain magnetic field but no electric field in the direction of propagation. Also known as H, or magnetic, waves.
- 4) Hybrid modes
Boundary conditions require all field components, may often be considered a coupling of TE and TM modes by the boundary conditions. Common in structures with "complex" 3-dimensional geometry.

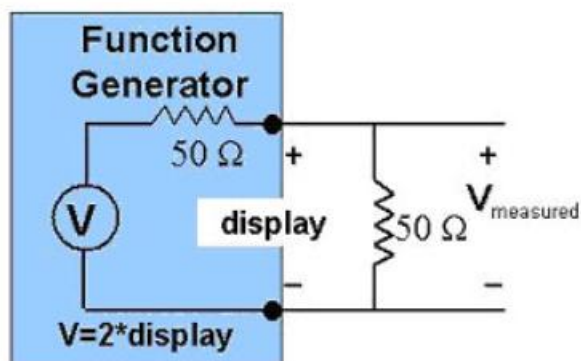
RF(AC)신호의 측정



Why your function generator outputs twice the programmed voltage

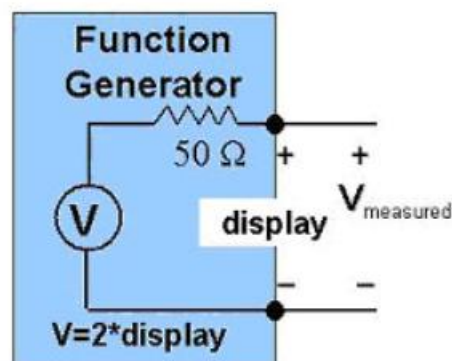
The default setting for Keysight function generators is to display the desired voltage as though terminated into a 50 Ohm load. When a high impedance device, such as an oscilloscope is used to measure the output of the function generator, the waveform appears to be twice the voltage set on the display of the oscilloscope.

Some oscilloscopes can change their input impedance from standard high impedance to a 50 Ohm termination. Another solution is to add a 50 Ohm feed through (Keysight part number: 0960-0301) to the end of the BNC cable.



$$V_{\text{measured}} = \frac{1}{2} V = \frac{1}{2} (2 * \text{display})$$

$$V_{\text{measured}} = \text{display}$$



$$V_{\text{measured}} = V = 2 * \text{display}$$

$$V_{\text{measured}} \neq \text{display}$$

Function generators tend to be signal generators that focus on low frequency, but with very flexible waveforms.

Signal generator is a more generic term, but would frequently refer to RF or audio frequency sine wave generators that are designed to generate signals with very high spectral purity and stable frequency and amplitude.